# Chapter IV Data Analysis



This chapter provides the analysis of the quantitative data. Case background will be firstly provided. A brief summary of the data analysis approach is described, including the statistical techniques employed. Next, the reliability and validity analysis of the survey instruments are presented. The results of the statistical analysis are discussed next. Finally, the case background is given with the summary of the findings. The set of acronyms used for the rest of this chapter is listed in Table 13.

Table 13 Acronyms of constructs

Construct Group	Acronym	Construct
User Acceptance	PU	Perceived Usefulness
	PEU	Perceived Ease of Use
	SN	Subjective Norm
	ATUC	Cognitive Attitude towards Usage
	ATUA	Affective Attitude towards Usage
	ATU	Attitude towards Usage
	IU	Intention to Use
	SA	Symbolic Adoption
User Resistance	PP	Perceived Level of Power
	PI	Perceived Inequity
	PSE	Perceived Self-efficacy
	RTAC	Cognitive Resistance Attitude
	RTAA	Affective Resistance Attitude
	RTA	Resistance Attitude
	RTB	Resistance Behaviors
Job-related Outcomes	JS	Job Satisfaction

# 4.1 Case background

Qualitative data were derived mainly from the interview sessions, with the additional information from news and documents. Data were summarized to illustrate the background of the case study. This will help to clarify the discussion of the results.

### 4.1.1 POSTAL Case Background Summary: A selection/definition phase

POSTAL is a large state-owned enterprise with the mission to provide postal and monetary services to the entire country. It was corporatized from another state-owned enterprise according to the policy of public reform. But before that, the first postal service in Thailand was introduced in 1883. With over a century of operation, the number of employees working for POSTAL was over 20,000. The services continued to serve the nationwide satisfactorily until the advancement of technology posed threats to the traditional services. The impact of technological change was clearly visible to POSTAL. People were offered with various choices of communication methods. They started to rely more on more advanced communication technologies such as e-mail rather than the conventional postal services. Notwithstanding the decline rate of customers, POSTAL strengthened the efficiency and reliability of services, as well as introduced new services for business and individual customers. Yummy Post was one of the examples. It is the service delivering Thai delicacies to any house in Bangkok, from all over Thailand. The reputation of POSTAL seemed to be better. It appeared that organizational change was not new to POSTAL, as it had been through radical transformation. This change was widely considered to be successful by others.

In the year 2008, there was an initiative to replace the old system with a new ERP package. The first attempt of the procurement was officially announced to the public in order to find a company to implement the new system. Unfortunately, the procurement was cancelled and postponed. Later, there were two consecutive attempts to procure the new ERP implementation, but both of the attempts were cancelled and postponed again. Finally, the fourth attempt was announced in May 2010. The data were collected shortly after the procurement was officially announced to the public. In spite of

lacking direct experience with the new implementation, they were aware of the forthcoming project. The old system being used was seen as providing benefits to the organization.

#### 4.1.2 ENERGY Case Summary: An implementation phase

The history of ENERGY, the other state-owned enterprise that served as a case in this study, began in the 1880s. With a long history of operation, organizational culture would present an obstacle to any change initiative. Change was also not new to this organization. In the year 1998 during the reign of Thaksin, there was an attempt at privatization. However, the idea of privatization was met with strong resistance from all quarters, particularly from labor unions. Strong resistance was demonstrated implicitly and explicitly. Despite the strong criticism against this change, the plan continued. After the exiled Prime Minister Thaksin was overthrown, the plan ceased. The consequential outcomes of privatization still yielded some benefits to ENERGY. An IT master plan was developed during the time of the privatization plan being executed. One of the IT initiatives was to implement an ERP project that could integrate all chains of commands in ENERGY as one unified system. In the year 2007, the ERP project began with the aim to integrate and streamline the working processes of all key functions. This was a big challenge to ENERGY since the organizational culture seemed to be a main barrier to the implementation. ENERGY had been operating in a form of a silo organization. There was no mutual standard of practice. Having operated under different principles for a long period of time, every business unit seemed to have different ideas in devising the new system. During the requirement definition phase, business blueprints were required to be developed as a new design of the integrated business process according to ASAP methodology. One of the milestones of this implementation project was business blueprints, for which users were to approve the design. When the due date of this milestone was approaching, there were disagreements from users with the new design. Users declined to sign off on the blueprint, causing a major delay of the entire project. A lot of effort was made to reconcile the disagreements. Although time limitation was enforced on users in dealing with the issues regarding the blueprint sign off, this

enforcement yielded controversial results. The progress of the project that seemed to be on hold for a certain period was pushed forward and the momentum of the project seemed to be recovered. Some groups of users agreed with this forceful approach, but others did not.

#### 4.1.3 WATER Case Summary: An operation phase

WATER, the state-owned enterprise founded in 1909, had the mission to provide good quality water supply to residences, businesses, and industries in Bangkok and the perimeter. Unlike the other two cases, no radical change was evidently identified close to the period of ERP implementation. The implementation of ERP had been completely finished for almost 10 years. The ERP was implemented within the original timeframe. Since the scope of the implementation was limited to only financial modules, it was viewed to be the reason that the implementation was finished on-time.

Only a few modules in accounting and finance were chosen to be implemented although ERP had been in use for a long period. Although there was a plan to upgrade the system to a new version, there still was no official plan to replace their older version of ERP. Users were familiar with the system, and the system usage became routine in this organization. Since it had been in operation quite long, the experiences from the implementation appeared not to affect the current usage although a few informants could remember what had happened during the implementation. Users acknowledged the benefits of using ERP. However, they thought that other modules should be implemented to cover more parts of business operations.

# 4.2 An approach to data analysis

The use of Structural Equation Modeling (SEM) has become more popular, since it incorporates several different statistical techniques including confirmatory factor analysis (CFA), path analysis, multiple regression analysis, and analysis of variance (ANOVA) (Bollen, 1995). The benefits of SEM overcome some limitations posed by traditional techniques. SEM can effectively deal with reciprocal relationships between constructs. Moreover, it allows a valid analysis of a model with latent variables. There are certain types of parameter estimation techniques used in SEM software: a covariance-based and component-based analysis (Chin, 1998a). In his comments on the use of SEM, Chin (1998a) suggests that a relatively large sample size should be considered in order for a model to provide sufficient statistical validity for a covariance-based approach to SEM as adopted in SEM software such as EQS and LISREL. Mainly, normal distributions of variables and the use of interval scale measures are assumptions that many of these approaches require.

Partial Least Squares (PLS) is a component approach to SEM distinct from the traditional factor-based covariance approaches (Chin, 1998a). It is seen to be a soft-modeling approach since few distribution assumptions are required (Tenenhaus et al., 2005). The use of PLS for estimating parameters in SEM is becoming more popular in IS research, as evidenced by the growing number of published articles in top-tier journals that employ the framework of TAM (e.g.,Gefen and Straub, 1997; Saadé and Bahli, 2005; Venkatesh and Morris, 2000; Venkatesh et al., 2003; Wixom and Todd, 2005). The reason underlying the growing popularity of SEM techniques is probably owing to the fact that this analytical approach is more useful when data size is comparatively small and multivariate normal distribution assumption is not achieved. In comparison to a covariance-based approach, assumptions in a PLS approach tend to be less restrictive (Henseler, Ringle, and Sinkovics, 2009; Tenenhaus et al., 2005).

Previous studies have informatively explained the details regarding the algorithm of PLS path models (Chin, 1998b; Henseler et al., 2009; Tenenhaus et al., 2005). In brief, path models are formally identified by the inner and outer models which

are often referred to as structural and measurement models. In an inner model, there are theorized pathways and relationships between unobserved or latent constructs. The relationships between a construct and the observed items are defined in a measurement model. After the PLS path models are defined, latent variable scores are estimated by an iterative procedure. At this stage, inner and outer weights are estimated in order to determine latent variable scores. The iteration process is terminated when the change in outer weights is less than the predefined threshold. Finally, loadings and inner regression coefficients are determined using a linear regression.

With all the benefits discussed above, it can be posited that PLS is a justified alternative choice for empirical research in IS. Theoretical models underpinning the theoretical framework proposed in this research comprise both structural and measurement models. Even though TAM can be seen to be a well-tested robust model, user resistance still lacks robust empirical validation and can be seen to be in the exploratory stage. Hence, in this study, a PLS approach to SEM was chosen for some justifiable reasons. smartPLS (Ringle, Wende, and Will, 2005) was used for this data analysis task. First, the sample size of this study is not relatively large. Second, some measures are not normally distributed. Third, this study aims to assess how effectively the proposed theories can predict and explain symbolic adoption and resistance to change, as well as job-related outcomes.

The steps in using PLS estimation for testing empirical data in the present study followed what is suggested by Henseler, et al. (2009). The measurement models were assessed for their reliability. Next, hypothesized relationships among theoretical constructs were tested. Data acquired from the three cases were used for model testing. To provide an exhaustive view of theory testing, theoretical models drawn from previous studies were empirically examined. These included TAM, Resistance to Change, and the proposed framework.

# 4.3 Reliability and Validity of Survey Instruments

Although there are no goodness-of-fit indices provided in a PLS approach to SEM, two primary criteria to assess the models have been recommended by Chin (1998b). The measurement reliability and validity should satisfy the cut-off criteria. The path models in this study were reflective measurement models, as all latent variables were measured by a combination of observed variables rather than the collective set of variables (Henseler et al., 2009). In this section, three sets of composite reliability and AVE (Average Variance Extracted) were obtained from three sets of data acquired from different cases in order to test the reliability and validity separately (for the detailed calculation of composite reliability and AVE, please see Henseler et al. (2009).

Composite reliability was primarily used to determine the degree of reliability of survey instruments adopted in this research instead of Cronbach's alpha, as the alpha was seen to underestimate the internal consistency reliability of latent variables in PLS path models. This follows what is suggested in the work of Henseler, et al. (2009) that summarizes previous studies related to PLS. The authors also recommend the criteria for assessing reflective measurement models. Composite reliability should not be lower than 0.6. When the composite reliability is low, an item can be excluded only if the exclusion substantially improves composite reliability.

Table 14 to Table 16 present composite reliability and AVE and Cronbach's alpha used to assess the reliability and validity of scales in path models from the three cases. All constructs from TAM passed the criterion suggested. However, some constructs from user resistance and job-related outcomes appear to have insufficient degree of reliability and validity in some cases.

For PI, the value of composite reliability was below 0.60 and the value of AVE was less than 0.50, in the case of POSTAL and WATER. PSE did not satisfy the cut-off criteria in the case of POSTAL and ENERGY. Furthermore, to provide a higher degree of reliability assessment, outer loadings of each item were reported in Table 17. It was

recommended that the value of loadings should be greater than 0.70 (Henseler et al., 2009).

Table 14 Summary of Composite Reliability and AVE: POSTAL

		Composite	AVE	Cronbach's
Construct Group	Acronym	Reliability		Alpha
User Acceptance	PU	0.940	0.722	0.881
	PEU	0.914	0.641	0.841
	SN	0.972	0.946	0.925
	ATUC	0.958	0.920	0.911
	ATUA	0.941	0.888	0.874
	ATU	0.954	0.839	0.936
	IU	0.940	0.838	0.932
	SA	0.878	0.707	0.791
User Resistance	PP	0.904	0.759	0.833
	PI	0.096	0.330	0.119
	PSE	0.255	0.199	0.798
	RTAC	0.907	0.765	0.841
	RTAA	0.968	0.884	0.956
	RTA	0.959	0.769	0.948
	RTB	0.716	0.509	0.703
Job-related Outcomes	JS	0.954	0.518	0.947

Table 15 Summary of Composite Reliability and AVE: ENERGY

		Composite	AVE	Cronbach's
Construct Group	Acronym	Reliability		Alpha
User Acceptance	PU	0.939	0.718	0.920
	PEU	0.927	0.678	0.893
	SN .	0.961	0.925	0.894
	ATUC	0.970	0.942	0.909
	ATUA	0.968	0.938	0.896
	ATU	0.968	0.885	0.957
	IU	0.955	0.875	0.914
	SA	0.946	0.853	0.854
User Resistance	PP	0.926	0.806	0.840
	PI	0.833	0.503	0.455
	PSE	0.690	0.384	0.737
	RTAC	0.908	0.767	0.794
	RTAA	0.952	0.832	0.917
	RTA	0.946	0.717	0.933
	RTB	0.820	0.491	0.669
Job-related Outcomes	JS	0.982	0.735	0.945

Table 16 Summary of Composite Reliability and AVE: WATER

	**************************************	Composite	AVE	Cronbach's
Construct Group	Acronym	Reliability		Alpha
User Acceptance	PU	0.951	0.765	0.935
	PEU	0.947	0.747	0.904
	SN	0.978	0.957	0.945
	ATUC	0.967	0.935	0.912
	ATUA	0.969	0.941	0.920
	ATU	0.972	0.895	0.950
	IU	0.964	0.900	0.932
	SA	0.933	0.822	0.858
User Resistance	PP	0.951	0.867	0.885
	PI	0.227	0.449	0.777
	PSE	0.899	0.748	0.821
	RTAC	0.960	0.856	0.788
	RTAA	0.942	0.702	0.937
	RTA	0.786	0.435	0.922
	RTB	0.933	0.775	0.728
Job-related Outcomes	JS	0.966	0.593	0.948



Table 17 Outer loadings of each item

Constructs	Items		Loadings	
		POSTAL	ENERGY	WATER
PU	PU1	0.847	0.830	0.867
	PU2	0.795	0.888	0.903
	PU3 <sup>-</sup>	0.839	0.874	0.911
	PU4	0.877	0.805	0.934
	PU5	0.860	0.839	0.878
	PU6	0.875	0.847	0.741
PEU	PEU1	0.830	0.812	0.843
	PEU2	0.875	0.840	0.848
	PEU3	0.850	0.839	0.897
	PEU4	0.764	0.800	0.910
	PEU5	0.669	0.841	0.850
	PEU6	0.798	0.809	0.836
SN	SN1	0.974	0.962	0.979
	SN2	0.971	0.962	0.978
ATUC	ATUC1	0.959	0.970	0.967
	ATUC2	0.959	0.971	0.967
ATUA	ATUA1	0.942	0.969	0.971
	ATUA2	0.943	0.968	0.969
ATU	ATUC1	0.918	0.930	0.949
	ATUC2	0.929	0.953	0.940
	ATUA1	0.904	0.944	0.959
	ATUA2	0.913	0.936	0.936
IU	IU1	0.899	0.934	0.932
	IU2	0.948	0.943	0.962
	IU3	0.900	0.930	0.952

Constructs	Items		Loadings	
		POSTAL	ENERGY	WATER
SA	SA1	0.875	0.941	0.922
	SA2	0.879	0.928	0.922
	SA3	0.764	0.902	0.875
PP	PP1	0.899	0.887	0.935
	PP2	0.934	0.915	0.945
	PP3	0.773	0.891	0.913
PI	PI1	0.627	0.723	-0.749
	PI2	0.674	0.871	-0.686
	PI3	-0.563	0.624	0.544
	PI4	0.417	0.698	-0.518
	PI5	-0.557	0.599	0.652
PSE	PSE1	0.761	0.619	0.876
	PSE2	0.396	0.629	0.898
	PSE3	0.104	0.260	0.855
	PSE4	-0.216	0.832	0.893
RTAC	RTAC1	0.778	0.855	0.825
	RTAC2	0.925	0.916	0.920
	RTAC3	0.913	0.855	0.847
RTAA	RTAA1	0.936	0.901	0.911
	RTAA2	0.940	0.932	0.946
	RTAA3	0.945	0.945	0.907
	RTAA4	0.939	0.868	0.937
RTA	RTAC1	0.778	0.867	0.632
	RTAC2	0.925	0.903	0.866
	RTAC3	0.913	0.904	0.781
	RTAA1	0.936	0.832	0.880

Constructs	Items	Loadings		
		POSTAL	ENERGY	WATER
	RTAA2	0.940	0.733	0.922
	RTAA3	0.945	0.847	0.857
	RTAA4	0.939	0.830	0.893
RTB	RTB1	0.636	0.447	0.382
	RTB2	0.637	0.827	0.800
	RTB3	0.645	0.801	0.680
	RTB4	0.578	0.816	0.680
	RTB5	-0.750	0.512	0.681
JS	JS1	0.394	0.671	0.619
	JS2	0.501	0.743	0.419
	JS3	0.720	0.839	0.736
	JS4	0.790	0.861	0.725
	JS5	0.583	0.837	0.736
	JS6	0.683	0.826	0.638
	JS7	0.552	0.839	0.817
	JS8	0.612	0.866	0.752
	JS9	0.785	0.881	0.844
	JS10	0.811	0.880	0.827
	JS11	0.842	0.902	0.818
	JS12	0.373	0.870	0.818
	JS13	0.714	0.900	0.826
	JS14	0.800	0.888	0.748
	JS15	0.689	0.875	0.731
	JS16	0.789	0.886	0.726
	JS17	0.845	0.878	0.905
	JS18	0.858	0.881	0.858

Constructs	Items	Loadings		
		POSTAL	ENERGY	WATER
	JS19		0.889	0.815
	JS20	0.863	0.895	0.898

As is evident from Tables 14 to 17, overall, the PI, PSE, and RTB did not satisfy the criteria of the reliability and validity of measurement models. Items with low loadings were dropped from the measurement models used in the three cases in order for the models to be applicable for comparison. These included PI3, PI4, PI5 from PI, PSE3, and PSE4 from PSE, and RTB5 from RTB as shown in Table 18.

Table 18 Decisions on dropping items

Construct	Items	English Questions	Thai Questions	Decision
PI	PI1	I invest more in my work	ฉันลงทุนในงานของฉัน	Kept
		than I get out of it.	มากกว่าที่ฉันได้จากงาน	
	PI2	I exert myself too much	ฉันทุ่มเทตัวเองมากเกินไป	Kept
		considering what I get	พิจารณากับสิ่งที่ฉันได้ตอบ	
		back in return.	แทนกลับมา	
	PI3	For the efforts I put into	สำหรับความพยายามที่ฉัน	Dropped
		the organization, I get	ได้ทุมเทไปกับองค์กรนี้ ฉัน	
		much in return.	ได้ผลตอบแทนกลับมามาก	
		(reversed)		
	PI4	If I take into account my	ถ้าฉันนำความทุ่มเทมา	Dropped
		dedication, the	พิจารณา องค์กรนี้ควรที่จะ	
		organization ought to	ให้การฝึกอบรมที่ดีกว่านี้	
		give me a better practical		
		training.		

Construct	Items	English Questions	Thai Questions	Decision
***************************************	PI5	In general, the benefits I	โดยทั่วไป ผลตอบแทนที่ฉัน	Dropped
		receive from the	ได้รับจากองค์กรนี้มีน้ำหนัก	
		organization outweigh the	มากกว่าสิ่งที่ฉันทุ่มเทลงไป	
		effort I put in it (reversed).		
PSE	PSE1	I could complete a job or	ฉันสามารถทำงานหรือ	Kept
		task using ERP if there is	ภารกิจให้สำเร็จโดยใช้ ERP	
		no one around to tell me	ถึงแม้ว่าไม่มีใครอยู่ใกล้ที่จะ	
		what to do as I go.	บอกฉันว่าฉันจะต้องทำอะไร	
	PSE2	I could complete a job or	ฉันสามารถทำงานหรือ	Kept
		task using ERP if I could	ภารกิจให้สำเร็จโดยใช้ ERP	
		call someone for help if I	ถ้าฉันสามารถเรียกถามคน	
		get stuck.	อื่นถ้าฉันใช้งานติดขัด	
	PSE3	I could complete a job or	ฉันสามารถทำงานหรือ	Droppe
		task using ERP if I have a	ภารกิจให้สำเร็จโดยใช้ ERP	
		lot of time to complete the	ถ้าฉันมีเวลามากมายเพื่อ	
		job for which ERP is	ทำงานที่จะต้องทำให้สำเร็จ	
		provided.	ใน ERP	
	PSE4	I could complete a job or	ฉันสามารถทำงานหรือ	Droppe
		task using ERP if I have	ภารกิจให้สำเร็จโดยใช้ ERP	
		just the built-in help	ถ้าฉันมีสิ่งอำนวยความ	
		facility for assistance.	สะดวกช่วยเหลือติดตั้งไว้	
			สำหรับการสนับสนุน	
RTB	RTB1	I look for ways to prevent	ฉันมองหาหนทางที่จะ	Kept
		ERP implementation.	ป้องกันการพัฒนาระบบ	
			ERP	
	RTB2	I protest against ERP	ฉันต่อต้านการพัฒนาระบบ	Kept
		implementation.	ERP	

Construct	Items	English Questions	Thai Questions	Decision
	RTB3	I complain about ERP	ฉันบ่นเกี่ยวกับการพัฒนา	Kept
		implementation to my	ระบบ ERP กับเพื่อน	
		colleagues.	ร่วมงานของฉัน	
	RTB4	I present my objections	ฉันเสนอความคิดคัดค้าน	Kept
		regarding ERP	เกี่ยวกับการพัฒนาระบบ	
		implementation to	ERP	
		management.		
	RTB5	I speak rather highly of	ฉันพูดเกี่ยวกับการพัฒนา	Dropped
		ERP implementation to	ระบบ ERP ในด้านดีกับผู้อื่น	
		others.		

After the exclusion of the items (details provided in Table 18), the models show improvement in the composite reliability and AVE, as shown in the Table 19. It may appear that the exclusion of the items would decrease the content validity. As these items were developed from other settings, they may not be applicable when used with this particular setting. The three organizations chosen for this study were state-owned enterprises providing infrastructure services. Members of this type of organization exhibited a particular type of behavior. In conclusion, all measurement models were considered to have satisfied the reliability.

Table 19 Summary of Composite Reliability and AVE: WATER

		Composite Reliability		A۱	/E
Constructs	CASE	Before	After	Before	After
		Exclusion	Exclusion	Exclusion	Exclusion
PI	POSTAL	0.096	0.886	0.330	0.795
	ENERGY	0.833	0.888	0.503	0.754
	WATER	0.227	0.938	0.449	0.883
PSE	POSTAL	0.255	0.852	0.199	0.744
	ENERGY	0.690	0.819	0.384	0.700
	WATER	0.933	0.910	0.776	0.836
RTB	POSTAL	0.716	0.890	0.509	0.671
	ENERGY	0.820	0.853	0.491	0.598
	WATER	0.786	0.881	0.435	0.654

Henseler et al. (2009) further recommend the assessment of validity. Convergent validity was assessed using Average Variance Extracted (AVE). A value of AVE should be higher than 0.5 for adequate convergent validity. Discriminant validity can be assessed by Fornell-Larcker criterion and cross-loadings. It was suggested that the AVE of each latent variable should be greater than the highest square of the latent variable to any other latent variable. As for the cross-loadings, an observed item should correlate higher with its latent variable than with others.

Table 20 to 22 present latent variable correlations and AVE on the diagonal. All constructs appear to have sufficient convergent validity since AVEs are greater than 0.50. Table 23 to 25 show cross-loadings. Most items are correlated highest with their particular latent variable. There are only two items that seem to be a problem. However, the highest cross-loadings of the problematic items to other latent variable were not much different from their loadings with their own latent variable. Therefore, it can be concluded that all constructs have adequate discriminant validity. In summary, all constructs satisfy the validity assessment.

Table 20 Latent variable correlations with AVE on the diagonal: POSTAL

	PU P	EU SN	Α	TU II		SA	PSE	PP	PI	R	TA	RTB	JS
PU	0.722												
PEU	0.844	0.641											
SN	0.714	0.737	0.946										
ATU	0.659	0.639	0.556	0.839									
IU	0.442	0.470	0.373	0.659	0.838								
SA	0.613	0.620	0.565	0.792	0.649	0.707							
PSE	0.472	0.417	0.381	0.639	0.548	0.584	0.74	4					
PP	0.046	0.186	0.201	0.194	0.217	0.201	0.26	9 0	.759				
PI	0.086	0.091	0.014	0.153	0.054	0.159	0.13	7 0	.496	0.795			
RTA	-0.094	0.081	0.140	-0.107	-0.161	0.022	-0.10	5 0	.415	0.304	0.769		
RTB	-0.137	-0.012	0.029	-0.063	0.071	-0.008	0.11	5 0	.361	0.276	0.494	0.67	1
JS	0.453	0.486	0.568	0.702	0.577	0.756	0.65	0 0	.306	0.216	0.170	0.208	0.518

Table 21 Latent variable correlations with AVE on the diagonal: ENERGY

	PU	PEU	SN	ATU	IU	SA	PSE	PP	PI	RTA	RTB	JS
PU	0.718											
PEU	0.732	0.678										
SN	0.523	0.578	0.925									
ATU	0.451	0.347	0.302	0.885								
IU	0.491	0.448	0.350	0.581	0.875							
SA	0.384	0.316	0.274	0.776	0.553	0.853						
PSE	0.370	0.422	0.262	0.406	0.504	0.369	0.700					
PP	0.249	0.260	0.184	0.283	0.231	0.303	0.252	0.806				
PI	0.131	0.141	0.163	0.282	0.187	0.327	0.224	0.361	0.754			
RTA	-0.142	-0.145	0.004	0.018	-0.175	0.122	-0.024	0.231	0.259	0.717		
RTB	-0.047	-0.032	0.026	-0.062	· -0.015	-0.021	0.038	0.291	0.128	0.562	0.598	
JS	0.321	0.273	0.268	0.499	0.330	0.586	0.289	0.347	0.304	0.253	0.115	0.735

Table 22 Latent variable correlations with AVE on the diagonal: WATER

	PU	PEU	SN	ATU	IU	SA	PSE	PP	PI	F	RTA	RTB	JS
PU	0.765												
PEU	0.787	0.747											
SN	0.605	0.637	0.957	•									
ATU	0.435	0.340	0.211	0.895									
IU	0.496	0.501	0.414	0.522	0.900								
SA	0.442	0.437	0.281	0.805	0.452	0.82	2						
PSE	0.315	0.402	0.340	0.104	0.137	0.22	4 0	.867					
PP	0.354	0.405	0.340	0.279	0.257	0.31	9 0	657	0.883				
PI	0.399	0.405	0.336	0.340	0.357	0.33	6 0	340	0.307	0.836			
RTA	-0.159	-0.164	-0.096	0.028	-0.188	0.14	8 0	298	0.186	-0.118	0.702		
RTB	0.046	0.037	-0.015	-0.079	0.157	-0.04	3 0	305	0.230	-0.156	0.495	0.654	
JS	0.551	0.482	0.450	0.618	0.535	0.62	9 0	289	0.382	0.522	0.079	0.132	0.593



Table 23 Cross-loadings: POSTAL

							-OCARU					
	PU	PEU	SN	UA	IU	SA	PSE	ower Ir	nequity	RC	RTC	JS
PU1	0.847	0.686	0.470	0.603	0.319	0.468	0.325	0.083	0.155	-0.124	-0.068	0.323
PU2	0.795	0.627	0.467	0.391	0.250	0.314	0.250	-0.023	0.045	-0.158	-0.169	0.164
PU3	0.840	0.713	0.702	0.505	0.400	0.515	0.408	0.014	0.014	-0.069	-0.136	0.440
PU4	0.877	0.750	0.587	0.555	0.372	0.528	0.432	0.005	0.065	-0.112	-0.112	0.360
PU5	0,860	0.742	0.687	0.636	0.462	0.622	0.481	0.046	0.069	-0.083	-0.130	0.539
PU6	0.875	0.766	0.683	0.624	0.408	0.609	0.461	0.090	0.087	0.035	-0.099	0.410
PEU1	0.743	0.830	0.588	0.549	0.456	0.494	0.417	0.198	0.054	-0.006	-0.057	0.425
PEU2	0.780	0.875	0.654	0.559	0.383	0.539	0.301	0.119	0.033	0.024	-0.065	0.397
PEU3	0.693	0.850	0.621	0.537	0.472	0.575	0.345	0.143	0.088	0.028	-0.062	0.460
	0.603	0.764	0.560	0.455	0.335	0.383	0.237	0.084	0.013	0.061	0.020	0.282
PEU4	8	600000000000000000000000000000000000000	0.523	0.433	0.333	0.374	0.236	0.139	0.175	0.328	0.166	0.291
PEU5	0.564	0.669			0.414	0.583	0.445	0.206	0.094	0.020	-0.006	0.453
PEU6	0.643	0.798	0.587	0.567					0.008	0.113	0.021	0.552
SN1	0.710	0.749	0.974	0.556	0.368	0.562	0.387	0.187	0.020	0.113	0.036	0.552
SN2	0.679	0.684	0.971	0.525	0.356	0.537	0.353	0.206				0.598
ATUA1	0.585	0.580	0.486	0.904	0.648	0.755	0.615	0.171	0.123	-0.164	-0.111	0.338
ATUA2	0.697	0.688	0.583	0.912	0.608	0.741	0.586	0.167	0.133	-0.021	-0.018	
ATUC1	0.607	0.555	0.471	0.919	0.606	0.689	0.531	0.138	0.114	-0.178	-0.079	0.568
ATUC2	0.522	0.514	0.494	0.929	0.552	0.717	0.610	0.236	0.192	-0.032	-0.025	0.689
IU1	0.419	0.462	0.368	0.537	0.901	0.542	0.485	0.161	-0.005	-0.157	0.091	0.518
IU2	0.431	0.443	0.397	0.654	0.947	0.635	0.559	0.237	0.053	-0.104	0.078	0.581
IU3	0.364	0.389	0.259	0.612	0.899	0.601	0.459	0.192	0.094	-0.186	0.028	0.485
SA1	0.560	0.555	0.489	0.658	0.523	0.880	0.491	0.181	0.136	0.116	-0.032	0.593
SA2	0.437	0.480	0.455	0.682	0.573	0.884	0.420	0.268	0.185	0.055	-0.010	0.659
SA3	0.550	0.528	0.481	0.656	0.538	0.755	0.563	0.055	0.077	-0.114	0.021	0.650
PSE1	0.411	0.376	0.302	0.540	0.468	0.488	0.929	0.260	0.127	-0.108	0.095	0.566
PSE2	0.419	0.350	0.388	0.594	0.501	0.553	0.791	0.197	0.108	-0.066	0.111	0.578
PP1	-0.064	0.030	0.059	0.042	0.115	0.072	0.142	0.899	0.407	0.390	0.311	0.170
PP2	0.063	0.222	0.225	0.167	0.192	0.182	0.249	0.934	0.455	0.415	0.348	0.269
PP3	0.168	0.278	0.286	0.382	0.311	0.336	0.371	0.773	0.458	0.248	0.283	0.429
PI1	0.120	0.111	-0.028	0.170	0.075	0.095	0.149	0.419	0,860	0.229	0.188	0.168
	0.120	0.059	0.044	0.113	0.028	0.178	0.103	0.463	0.923	0.304	0.292	0.213
PI2			0.177	0.020	-0.083	0.065	-0.091	0.419	0.295	0.928	0.438	0.168
RTAA1	-0.058	0.118			-0.194	0.003	-0.091	0.392	0.300	0,935	0.469	0.147
RTAA2	-0.096	0.072	0.159	-0.116 -0.098	-0.099	0.021	-0.084	0.352	0.286	0.901	0.388	0.182
RTAA3	-0.083	0.050	0.125			0.057	-0.122	0.330	0.214	0.900	0.415	0.177
RTAA4	-0.045	0.082	0.118	-0.065	-0.080				0.198	0.694	0.395	0.115
RTAC1	-0.017	0.125	0.103	-0.056	-0.134	0.062	0.005	0.256		0.899	0.497	0.136
RTAC2	-0.100	0.065	0.093	-0.126	-0.164	-0.034	-0.112	0.350	0.236	SEC. 17. 250 SEC. 200		0.116
RTAC3	-0.163	-0.007	0.077	-0.213	-0.232	-0.059	-0.128	0.427	0.324	0.859	0.429	
RTB1	0.064	0.178	0.113	0.118	0.339	0.119	0.286	0.447	0.151	0.263	0.719	0.240
RTB2	-0.191	-0.108	-0.026	-0.150	-0.054	-0.118	0.010	0.317	0.226	0.484	0.896	0.133
RTB3	-0.092	-0.065	0.065	-0.015	0.009	0.047	0.126	0.216	0.318	0.389	0.781	0.224
RTB4	-0.176	0.015	-0.025	-0.105	0.027	-0.028	0.021	0.251	0.200	0.449	0.871	0.116
JS1	0.162	0.217	0.192	0.240	0.187	0.284	0.118	0.196	0.455	0.294	0.217	0.401
JS2	0.183	0.235	0.289	0.240	0.171	0.280	0.270	0.179	0.308	0.293	0.189	0.505
JS3	0.347	0.319	0.554	0.483	0.270	0.519	0.447	0.162	0.101	0.196	0.110	0.721
JS4	0.363		0.546	0.540	0.431	0.720	0.421	0.282	0.172	0.208	0.165	0.795
JS5	0.147		0.218	0.292	0.311	0.338	0.300	0.398	0.361	0.356	0.251	0.587
JS6	0.335		0.247	0.497	0.377		0.465	0.208	0.258	0.048	0.094	0.684
JS7	0.171		0.203	0.363	0.312		0.311	0.251	0.156	0.195	0.133	0.556
158	0.140		0.256	0.350	0.239		0.370	0.108	0.075	0.147	0.175	0.612
	0.435		0.530	0.662	0.549		0.478	0.185	0.100	0.140	0.117	0.785
JS9	0.433		0.534	0.534	0.391		0.465	0.193	0.098	0.202	0.128	0.813
JS10							0.556	0.227	0.091	0.113	0.125	0.842
JS11	0.340		0.494						0.158	0.169	0.394	0.380
JS12	0.128		0.208				0.238	0.322			0.103	0.711
JS13	0.365						0.537	0.147	0.026	-0.046		0.70405.2000960600000
JS14	0.458							0.259	0.234	0.044	0.133	0.799
JS15	0.391							0.255	0.095	0.016	0.084	0.686
JS16	0.380							0.320	0.120	0.063	0.160	0.787
JS17	0.353	0.331	0.429	0.601	0.458			0.169	0.117	0.106	0.150	0.840
JS18	0.356	0.361	0.430	0.643	0.477	0.631	0.563	0.257	0.193	0.067	0.139	0.855
JS19	0.448				0.557	0.649	0.640	0.246	0.136	0.101	0.213	0.00000.0000000000000000000000000000000
JS20	0.377						0.627	0.156	0.152	0.059	0.156	0.861
7320	0.377	0.505	5. 100	2.000								

Table 24 Cross-loadings: ENERGY

	PU	PEU	SN	UA	IU	SA	PSE	Inequity	Power	RC	RTC	JS
PU1	0.831	0.573	0.391	0.392	0.344	0.385	0.297	0.209	0.162	-0.083	-0.026	0.270
PU2	0.888	0.629	0.371	0.449	0.333	0.485	0.329	0.206	0.110	-0.160	-0.043	0.262
PU3	0.874	0.625	0.368	0.432	0.299	0.375	0.300	0.232	0.092	-0.113	-0.060	0.264
PU4	0.805	0.522	0.381	0.372	0.350	0.377	0.263	0.246	0.170	-0.090	-0.030	0.310
PU5	0.839	0.670	0.425	0.520	0.329	0.477	0.332	0.171	0.063	-0.163	-0.045	0.278
PU6	0.847	0.686	0.354	0.482	0.302	0.386	0.355	0.209	0.078	-0.107	-0.034	0.249 0.197
PEU1	0.619	0.812	0.254	0.421	0.264	0.340	0.364	0.236	0. <b>117</b> 0. <b>099</b>	-0.122 -0.146	0.000 -0.037	0.197
PEU2	0.638	0.840	0.316	0.466	0.302	0.375 0.388	0.351 0.350	0.209 0.212	0.147	-0.170	-0.057	0.257
PEU3	0.582	0.839	0.301 0.248	0.466 0.480	0.256 0.228	0.367	0.330	0.160	0.062	-0.065	-0.037	0.194
PEU4	0.561 0.620	0.800 0.841	0.248	0.487	0.254	0.374	0.359	0.246	0.099	-0.090	0.013	0.203
PEU5 PEU6	0.592	0.809	0.307	0.536	0.252	0.373	0.360	0.216	0.173	-0.120	-0.049	0.250
SN1	0.383	0.277	0.930	0.262	0.698	0.542	0.371	0.242	0.245	0.000	-0.066	0.429
SN2	0.443	0.340	0.953	0.301	0.721	0.554	0.387	0.257	0.243	0.018	-0.022	0.454
ATUA1	0.501	0.560	0.301	0.962	0.266	0.340	0.257	0.194	0.157	-0.014	0.025	0.266
ATUA2	0.506	0.551	0.279	0.962	0.260	0.332	0.248	0.159	0.157	0.021	0.025	0.249
ATUC1	0.424	0.330	0.277	0.944	0.730	0.535	0.395	0.268	0.288	0.031	-0.068	0.478
ATUC2	0.445	0.354	0.294	0.936	0.767	0.555	0.374	0.296	0.284	0.017	-0.078	0.515
IU1	0.338	0.277	0.698	0.231	0.941	0.517	0.333	0.293	0.324	0.131	-0.011	0.549
IU2	0.341	0.291	0.701	0.260	0.929	0.502	0.342	0.291	0.277	0.124	0.026	0.515
IU3	0.385	0.306	0.747	0.267	0.900	0.511	0.347	0.257	0.304	0.083	-0.071	0.558
SA1	0.468	0.425	0.555	0.321	0.523	0.933	0.479	0.240	0.179	-0.173	-0.036	0.311
SA2	0.463	0.414	0.543	0.332	0.496	0.940	0.477	0.177	0.151	-0.180	-0.026	0.296
SA3	0.446	0.419	0.532	0.329	0.529	0.933	0.459	0.230	0.194	-0.140	0.017	0.319
PSE1	0.341	0.385	0.352	0.224	0.302	0.449	0.974		0.193	-0.026	0.057	0.247
PSE2	0.313	0.369	0.413	0.279	0.435	0.475	0.673	2002/06/08/09/09/09/09	0.232	-0.008	-0.041	0.307
PP1	0.179	0.221	0.201	0.143	0.219	0.194	0.225	3500 (300 SHB) (350 SH	0.345	0.227	0.299	0.297
PP2	0.229	0.214	0.265	0.172	0.274	0.213	0.218	52401 (0.0000000000000000000000000000000000	0.311	0.205	0.251 0.228	0.306 0.336
PP3	0.272	0.269	0.306	0.183	0.334	0.217	0.237		MODELS OF THE PARTY OF	0.187 0.147	0.063	0.330
PI1	0.181	0.192	0.269	0.142	0.328	0.251	0.223		SULCOUNTED STREET	0.147	0.145	0.286
PI2	0.087	0.096	0.251	0.153	0.282	0.129	0.195 -0.019			0.868	0.506	0.255
RTAA1	-0.094	-0.072	0.060	0.037 -0.041	0.133	-0.131 -0.181	-0.050		0.198	0.903	0.506	0.194
RTAA2	-0.153	-0.148	-0.034 0.011	-0.041	0.047	-0.208	-0.079			0.904	0.478	0.199
RTAA3	-0.134	-0.144 -0.146	-0.015	0.067	0.068	-0.166	-0.078			0.833	0.463	0.150
RTAA4	-0.110 -0.031	-0.146	0.092	0.033	0.145	-0.068	0.079		3	0.732	0.424	0.229
RTAC1	-0.031	-0.120	-0.044	-0.003	0.124	-0.150	0.029			0.846	0.499	0.217
RTAC2 RTAC3	-0.145	-0.178	0.047	-0.027	0.130	-0.126	-0.017			0.830	0.448	0.259
RTB1	0.180	0.217	0.167	0.225	0.135	0.300	0.229			0.191	0.528	0.215
RTB2	-0.056	-0.025	-0.096	-0.008	-0.084	-0.084	0.040			0.496	0.866	0.077
RTB3	-0.127	-0.142	-0.115	0.013	-0.066	-0.034	-0.026		0.073	0.479	0.820	0.030
RTB4	-0.028	-0.022	-0.034	-0.033	0.032	-0.058	-0.014		0.144	0.486	0.832	0.113
JS1	0.157	0.124	0.284	0.251	0.336	0.146	0.151	0.176	0.254	0.299	0.162	0.670
JS2	0.182	0.149	0.360	0.157	0.395	0.219	0.271	0.225	0.286	0.233	0.081	0.744
JS3	0.230		0.460	0.192	0.514	0.286	0.241			0.238	0.053	0.839
JS4	0.255		0.430	0.248	0.512	0.291	0.286			0.264	0.129	0.862
JS5	0.268	0.191	0.408	0.208	0.444	0.244	0.230			0.248	0.104	0.836
JS6	0.239	0.198	0.434	0.196	0.478	0.288	0.304			0.232	0.108	0.825
JS7	0.215	0.192	0.409	0.203	0.446	0.219	0.237			0.270	0.123	0.839
JS8	0.241	0.209	0.422	0.167	0.491	0.265	0.208			0.248	0.148	0.865
JS9	0.253	0.197	0.447	0.179			0.226			0.199	0.090	0.881
JS10	0.287	0.239	0.437	0.254		0.300	0.250			0.196		0.880
JS11	0.300		0.448	0.226			0.230			0.199		0.902
JS12	0.304		0.503	0.238			0.249			0.170		0.871
JS13	0.316		0.438				0.24					50 (0.000) 2000
JS14	0.338		0.446				0.26					500000000000000000000000000000000000000
JS15	0.301		0.407									500000000000000000000000000000000000000
JS16	0.326		0.423									
JS17	0.322		0.454									100000000000000000000000000000000000000
JS18	0.293											
JS19	0.293											530000000000000000000000000000000000000
JS20	0.319	0.263	0.448	0.253	0.509	0.306	0.26	8 0.31	0.242	0.156	0.102	0.894

Table 25 Cross-loadings: WATER

Puil	-	PU	PEU	SN	UA	IU	SA	PSE	Inequity	Power	RC	RTC	JS
PUZ   0.093	PU1												0.433
PIMS   0.958   0.766   0.544   0.436   0.491   0.443   0.285   0.298   0.400   0.182   0.254   0.499     PIMS   0.741   0.593   0.516   0.395   0.485   0.413   0.312   0.218   0.307   0.067   0.202   0.389     PIMS   0.741   0.593   0.516   0.310   0.312   0.465   0.313   0.180   0.407   0.407   0.313   0.180   0.313   0.410   0.407   0.315   0.325   0.322   0.349   0.416   0.221   0.399     PIMS   0.677   0.697   0.588   0.359   0.490   0.400   0.266   0.328   0.355   0.194   0.223   0.389     PIMS   0.677   0.697   0.588   0.359   0.490   0.400   0.266   0.328   0.355   0.194   0.223   0.349     PIMS   0.677   0.697   0.588   0.359   0.490   0.400   0.266   0.328   0.355   0.194   0.223   0.442     PIMS   0.677   0.697   0.581   0.599   0.490   0.400   0.660   0.328   0.355   0.194   0.223   0.442     PIMS   0.677   0.689   0.611   0.515   0.399   0.309   0.405   0.288   0.255   0.355   0.316   0.219   0.423     PIMS   0.697   0.685   0.697   0.339   0.325   0.325   0.251   0.283   0.412   0.109   0.455     SIN1   0.594   0.655   0.6978   0.203   0.382   0.276   0.251   0.283   0.412   0.109   0.455     SIN1   0.595   0.611   0.698   0.610   0.328   0.276   0.338   0.486   0.293   0.009   0.405     SIN1   0.595   0.611   0.698   0.610   0.788   0.595   0.335   0.380   0.608   0.385   0.586     ATUAL   0.398   0.302   0.167   0.595   0.482   0.799   0.738   0.263   0.389   0.400   0.385		0,903	0.660	0.504	0.415	0.387	0.393	0.236	0.304	0.237	-0.096	-0.118	0.460
PUS	PU3	0.911	0.757	0.547	0.368	0.485	0.392	0.337	0.357	0.340	-0.167	-0.274	0.526
Pug	PU4	0.934	0.766	0.544	0.436	0.491	0.443	0.285	0.298	0.400	-0.182	-0.254	
PEUIZ 0.664 0.845 0.464 0.313 0.410 0.407 0.344 0.404 0.331 -0.089 0.160 0.427 0.424 0.727 0.845 0.548 0.329 0.432 0.355 0.326 0.322 0.349 0.143 0.0239 0.399 0.490 0.406 0.266 0.322 0.349 0.143 0.023 0.424 0.424 0.693 0.970 0.857 0.548 0.359 0.909 0.405 0.328 0.325 0.316 0.159 0.223 0.429 0.42	PU5	0.878	0.711	0.586	0.358	0.485	0.413						
Puls		80	THE PROPERTY OF THE PROPERTY OF										
Pusus		28	1770309888889855										
FULM         0.693         0.910         0.621         0.305         0.471         0.415         0.462         0.305         0.316         0.129         0.485           PEUS         0.607         0.836         0.516         0.229         0.398         0.285         0.277         0.283         0.114         0.105         0.348           SN1         0.697         0.835         0.516         0.229         0.382         0.277         0.233         0.234         0.110         0.040         0.348           SN1         0.699         0.611         0.789         0.020         0.327         0.233         0.293         -0.099         0.021         0.040           ATUAL         0.396         0.320         0.125         0.940         0.461         0.472         0.071         0.353         0.389         0.302         0.156         0.935         0.922         0.472         0.071         0.355         0.344         0.080         0.366         0.357         0.093         0.402         0.052         0.365         0.362         0.344         0.090         0.402         0.462         0.352         0.365         0.325         0.042         0.532         0.365         0.422         0.377		2	079 9400 320 300 300 300										
Peus		W	334000000000000000000000000000000000000										
PEUG		3	519573 (\$79927) \$1956										
SN1         0.594         0.651         0.978         0.213         0.288         0.280         0.327         0.288         0.293         -0.109         -0.211         0.485           ATUA1         0.405         0.326         0.194         0.549         0.501         0.788         0.079         0.338         0.289         -0.089         -0.385         0.386           ATUA2         0.398         0.320         0.151         0.999         0.492         0.670         0.417         0.389         0.038         0.226         0.036         0.325         0.492         0.636         0.032         0.494         0.338         0.224         0.995         0.492         0.665         0.085         0.355         0.340         0.080         0.327         0.466         0.365         0.082         0.235         0.408         0.221         0.416         0.418         0.436         0.821         0.055         0.082         0.235         0.366         0.227         0.334         0.012         0.112         0.531         0.902         0.466         0.155         0.229         0.334         0.131         0.122         0.131         0.234         0.235         0.406         0.155         0.260         0.235         0.20		7	000000000000000000000000000000000000000										
SNE				NON NECESSARIA (CONTRACTOR)									
ATUAL				100000000000000000000000000000000000000									
ATUCI 0.398 0.320 0.215 0.940 0.463 0.742 0.071 0.346 0.355 0.039 -0.342 0.588 ATUCI 0.396 0.302 0.167 0.959 0.492 0.769 0.147 0.355 0.335 0.344 0.080 0.305 0.5788 ATUCI 0.449 0.338 0.224 0.998 0.518 0.745 0.095 0.355 0.302 0.045 0.328 0.699 IUI 0.470 0.489 0.375 0.462 0.992 0.366 0.062 0.235 0.366 0.217 0.112 0.513 IUI 0.481 0.486 0.367 0.523 0.962 0.466 0.165 0.299 0.374 0.134 0.137 0.513 IUI 0.481 0.486 0.367 0.523 0.962 0.466 0.165 0.299 0.374 0.134 0.137 0.513 IUI 0.481 0.486 0.367 0.523 0.962 0.466 0.165 0.299 0.374 0.134 0.137 0.513 IUI 0.481 0.486 0.367 0.523 0.962 0.466 0.185 0.299 0.387 0.392 0.166 0.528 0.366 0.127 0.107 0.076 0.588 0.407 0.388 0.499 0.387 0.799 0.769 0.688 0.408 0.922 0.133 0.302 0.245 0.171 0.246 0.101 0.533 0.429 0.387 0.799 0.769 0.436 0.875 0.767 0.378 0.379 0.391 0.062 0.425 0.554 0.595 0.385 0.385 0.393 0.393 0.393 0.393 0.393 0.393 0.394 0.389 0.389 0.389 0.389 0.507 0.391 0.062 0.422 0.554 0.591 0.391 0.				38	9808/987628/9878782808080800000000000000000000000000								
ATUCI 0.396 0.302 0.167 0.959 0.492 0.769 0.147 0.355 0.344 0.080 0.306 0.578 ATUCI 0.449 0.338 0.224 0.996 0.518 0.776 0.095 0.355 0.302 0.045 0.035 0.609 IUI 0.470 0.439 0.375 0.462 0.932 0.365 0.082 0.235 0.366 0.217 0.011 0.513 IUZ 0.481 0.486 0.367 0.523 0.962 0.466 0.165 0.299 0.374 0.134 0.137 0.508 IU3 0.461 0.487 0.488 0.497 0.952 0.466 0.165 0.299 0.374 0.134 0.137 0.508 SA1 0.387 0.354 0.211 0.728 0.384 0.922 0.449 0.137 0.522 0.335 0.192 0.125 0.506 SA2 0.384 0.449 0.776 0.688 0.408 0.922 0.297 0.324 0.289 0.168 0.277 0.526 0.546 SA3 0.429 0.387 0.729 0.769 0.436 0.875 0.176 0.297 0.319 0.062 0.442 0.558 PSEZ 0.317 0.330 0.349 0.122 0.107 0.097 0.133 0.935 0.507 0.215 0.309 0.183 0.173 PSEZ 0.317 0.330 0.349 0.122 0.120 0.223 0.945 0.507 0.215 0.309 0.183 0.173 PSP1 0.333 0.356 0.337 0.203 0.169 0.288 0.339 0.644 0.795 0.385 0.151 0.007 0.315 PP2 0.355 0.415 0.378 0.309 0.288 0.339 0.644 0.795 0.385 0.151 0.009 0.428 PP3 0.317 0.355 0.475 0.375 0.275 0.276 0.206 0.206 0.270 0.598 0.716 0.316 0.193 0.093 0.438 PI1 0.411 0.463 0.368 0.288 0.343 0.328 0.261 0.445 0.876 0.112 0.339 0.488 PI2 0.306 0.251 0.230 0.349 0.190 0.118 0.212 0.192 0.227 0.077 0.135 0.059 0.488 RTAA1 0.032 0.104 0.030 0.190 0.118 0.120 0.273 0.188 0.445 0.876 0.112 0.339 0.488 PI2 0.306 0.251 0.230 0.342 0.307 0.273 0.188 0.445 0.876 0.012 0.051 0.451 0.466 RTAA2 0.139 0.154 0.0159 0.081 0.130 0.115 0.234 0.203 0.086 0.886 0.354 0.044 RTAA3 0.100 0.153 0.024 0.008 0.004 0.180 0.185 0.185 0.166 0.022 0.041 0.058 0.007 0.135 0.155 0.009 0.183 0.009 0.033 0.185 0.185 0.000 0.150 0.100 0.150 0.008				18									
ATUC2					201000000000000000000000000000000000000								
IU1				- 20	97.8 S.								
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NA					100	2012013/08/2002/09/2002		0.165	0.299	0.374	-0.134	-0.137	0.508
\$A2 0.384 0.449 0.276 0.688 0.408 0.922 0.297 0.324 0.289 0.168 -0.270 0.546 \$A3 0.429 0.387 0.279 0.769 0.436 0.875 0.176 0.297 0.391 0.062 0.422 0.554 \$A3 0.429 0.387 0.279 0.769 0.436 0.875 0.176 0.297 0.391 0.062 0.422 0.554 \$A5 0.228 0.317 0.370 0.349 0.122 0.120 0.223 0.945 0.530 0.244 0.250 0.070 0.315 \$PEZ 0.317 0.370 0.349 0.122 0.120 0.223 0.945 0.530 0.244 0.250 0.070 0.315 \$PEZ 0.355 0.415 0.338 0.393 0.203 0.169 0.284 0.933 0.600 0.324 0.266 0.044 0.329 \$PEZ 0.355 0.415 0.338 0.399 0.828 0.339 0.644 0.795 0.385 0.151 0.000 0.428 \$PEZ 0.355 0.415 0.338 0.399 0.388 0.339 0.644 0.795 0.385 0.151 0.000 0.428 \$PEZ 0.306 0.251 0.230 0.342 0.307 0.273 0.388 0.428 0.898 0.399 0.848 0.399 0.848 0.399 0.844 0.795 0.385 0.258 0.345 0.368 0.388 0.398 0.464 0.795 0.385 0.455 0.396 0.442 0.459 0.428 0.489 0.491 0.491 0.461 0.463 0.368 0.288 0.339 0.288 0.339 0.644 0.405 0.376 0.316 0.133 0.093 0.303			0.497	0.438	26	0.952	0.449	0.137	0.252	0.335	-0.192	-0.125	0.506
SA3         0.429         0.387         0.279         0.769         0.436         0.875         0.176         0.297         0.391         0.062         -0.422         0.554           PSE1         0.238         0.361         0.272         -0.017         0.097         0.133         0.335         0.507         0.215         0.309         0.183         0.175           PF1         0.333         0.396         0.337         0.203         0.169         0.284         0.913         0.600         0.324         0.266         0.044         0.329           PP2         0.355         0.415         0.378         0.399         0.288         0.339         0.644         0.795         0.385         0.151         0.005         0.428           PP3         0.317         0.355         0.275         0.226         0.206         0.270         0.998         0.795         0.385         0.151         0.000         0.030         0.303         0.303         0.303         0.334         0.044         0.036         0.086         0.086         0.081         0.010         0.027         0.088         0.042         0.061         0.186         0.032         0.061         0.186         0.032         0.061 <th< th=""><th>SA1</th><th>0.387</th><th>0.354</th><th>0.211</th><th>0.728</th><th>0.384</th><th>0.922</th><th>0.143</th><th>0.302</th><th>0.245</th><th>0.171</th><th>-0.246</th><th>0.610</th></th<>	SA1	0.387	0.354	0.211	0.728	0.384	0.922	0.143	0.302	0.245	0.171	-0.246	0.610
PSE1 0.238 0.361 0.272 -0.017 0.097 0.133 0.935 0.507 0.215 0.309 0.183 0.173   PSE2 0.317 0.370 0.349 0.122 0.120 0.223 0.945 0.530 0.244 0.250 0.070 0.315   PP1 0.333 0.396 0.337 0.203 0.169 0.284 0.913 0.600 0.324 0.266 0.044 0.329   PP2 0.355 0.415 0.378 0.309 0.288 0.339 0.644 0.795 0.385 0.151 -0.005 0.428   PP3 0.317 0.355 0.275 0.226 0.206 0.270 0.598 0.716 0.316 0.193 0.093 0.303   PP1 0.411 0.463 0.368 0.288 0.343 0.328 0.644 0.455 0.876 0.316 0.193 0.093 0.303   PP1 0.411 0.463 0.368 0.288 0.343 0.328 0.616 0.445 0.876 0.316 0.193 0.093 0.303   PP1 0.306 0.251 0.230 0.342 0.307 0.273 0.188 0.428 0.898 0.092 0.451 0.466   RTAA1 0.032 0.104 0.030 0.190 0.118 0.212 0.192 0.227 0.073 0.652 0.061 0.186   RTAA2 0.139 0.154 0.159 0.081 0.0130 0.115 0.224 0.023 0.066 0.866 0.354 0.044   RTAA3 0.100 0.153 0.024 0.088 0.084 0.168 0.341 0.275 0.050 0.781 0.352 0.129   RTAA4 0.014 0.001 0.027 0.008 0.131 0.155 0.337 0.210 0.207 0.879 0.455 0.073   RTAC1 0.176 0.127 0.134 0.027 0.168 0.100 0.235 0.185 0.165 0.029 0.455 0.078   RTAC2 0.222 0.010 0.058 0.010 0.217 0.087 0.188 0.184 0.097 0.857 0.415 0.065   RTAC3 0.228 0.229 0.169 0.115 0.074 0.315 0.155 0.346 0.346 0.077 0.099 0.222 0.330   RTB3 0.085 0.077 0.026 0.054 0.155 0.078 0.125 0.278 0.032 0.090 0.222 0.330   RTB3 0.085 0.077 0.026 0.054 0.155 0.078 0.125 0.208 0.132 0.397 0.660 0.138   ISS 0.361 0.361 0.360 0.308 0.459 0.025 0.078 0.135 0.060 0.344 0.367 0.362 0.079 0.097 0.222 0.330 0.315 0.351 0.352 0.150 0.352 0.138 0.351 0.352 0.079 0.097 0.222 0.330 0.340 0.355 0.351 0.351 0.350 0.366 0.364 0.377 0.073 0.060 0.225 0.385 0.377 0.207 0.097 0.222 0.330 0.115 0.352 0.351 0.351 0.350 0.351 0.351 0.350 0.350 0.364 0.377 0.025 0.060 0.314 0.344 0.354 0.350 0.351 0.350 0.351 0.350 0.351 0.351 0.350 0.351 0.350 0.351 0.350 0.351 0.351 0.350 0.351 0.351 0.351 0.350 0.350 0.364 0.377 0.022 0.352 0.351	SA2	0.384	0.449	0.276	0.688	0.408	0.0000000000000000000000000000000000000	0.297	0.324	0.289			
PSEZ         0.317         0.370         0.349         0.122         0.120         0.223         0.945         0.530         0.244         0.250         0.070         0.315           PP1         0.333         0.396         0.337         0.203         0.169         0.284         0.913         0.600         0.324         0.266         0.044         0.329           PP2         0.355         0.415         0.378         0.388         0.339         0.644         0.795         0.385         0.151         0.005         0.428           PP3         0.317         0.355         0.275         0.226         0.206         0.270         0.598         0.716         0.316         0.193         0.093         0.303           P11         0.411         0.463         0.388         0.388         0.388         0.388         0.389         0.218         0.018         0.121         0.121         0.122         0.031         0.033         0.044         0.021         0.122         0.073         0.682         0.068         0.884         0.186         0.431         0.227         0.066         0.284         0.034         0.224         0.034         0.024         0.027         0.087         0.028	SA3	0.429	0.387	0.279	0.769	0.436	0.875	0.176	0.297				
PP1 0.333 0.396 0.337 0.203 0.169 0.284 0.913 0.600 0.324 0.266 0.044 0.329 PP2 0.355 0.415 0.378 0.309 0.288 0.339 0.644 0.795 0.385 0.151 0.005 0.428 PP3 0.317 0.355 0.275 0.226 0.206 0.270 0.598 0.716 0.316 0.193 0.093 0.033 P11 0.411 0.463 0.368 0.288 0.343 0.328 0.261 0.445 0.876 0.121 0.330 0.488 P12 0.306 0.251 0.230 0.342 0.307 0.273 0.188 0.428 0.899 0.092 0.451 0.466 RTAA1 0.032 0.104 0.030 0.190 0.118 0.212 0.192 0.227 0.073 0.652 0.066 0.354 RTAA2 0.139 0.154 0.159 0.081 0.130 0.115 0.234 0.203 0.086 0.866 0.354 0.044 RTAA3 0.100 0.153 0.024 0.088 0.088 0.084 0.168 0.341 0.275 0.050 0.781 0.352 0.129 RTAA4 0.014 0.001 0.027 0.008 0.131 0.155 0.337 0.210 0.207 0.579 0.455 0.078 RTAC2 0.176 0.127 0.134 0.027 0.168 0.100 0.235 0.185 0.166 0.922 0.450 0.001 RTAC2 0.222 0.201 0.058 0.010 0.217 0.087 0.188 0.184 0.097 0.857 0.415 0.065 RTAC3 0.228 0.229 0.169 0.115 0.250 0.660 0.214 0.184 0.198 0.857 0.455 0.005 RTB1 0.191 0.181 0.021 0.074 0.315 0.165 0.346 0.207 0.009 0.222 0.322 0.329 RTB2 0.023 0.018 0.000 0.160 0.019 0.099 0.271 0.148 0.198 0.520 0.222 0.332 0.115 STS1 0.033 0.339 0.372 0.054 0.155 0.060 0.215 0.208 0.146 0.199 0.271 0.18 0.199 0.154 0.199 0.222 0.332 0.169 0.051 0.051 0.059 0.271 0.18 0.109 0.271 0.18 0.199 0.271 0.18 0.199 0.271 0.18 0.007 0.009 0.222 0.332 0.112 0.007 0.009 0.222 0.332 0.112 0.007 0.009 0.222 0.332 0.113 0.000 0.009 0.009 0.271 0.18 0.009 0.222 0.332 0.113 0.000 0.009 0.009 0.271 0.18 0.000 0.009 0.222 0.332 0.113 0.000 0.	PSE1	0.238	0.361	0.272	-0.017	0.097							
PP2         0.355         0.415         0.378         0.309         0.288         0.339         0.644         0.795         0.385         0.151         -0.005         0.428           PP3         0.317         0.355         0.275         0.226         0.206         0.270         0.598         0.736         0.315         0.193         0.093         0.303           P11         0.411         0.463         0.368         0.288         0.343         0.328         0.261         0.445         0.876         -0.121         -0.330         0.488           P12         0.306         0.251         0.030         0.190         -0.118         0.212         0.192         0.227         0.073         0.632         0.061         0.186           RTAA1         -0.139         -0.153         -0.024         0.088         -0.084         0.168         0.341         0.275         0.050         0.781         0.352         0.128           RTAA3         0.100         0.153         -0.024         0.088         -0.131         0.155         0.337         0.275         0.050         0.781         0.352         0.128           RTAA3         0.016         0.001         0.021         0.087 <t< th=""><th>PSE2</th><th>0.317</th><th>0.370</th><th>0.349</th><th></th><th></th><th></th><th>71.900000000000000</th><th></th><th></th><th></th><th></th><th></th></t<>	PSE2	0.317	0.370	0.349				71.900000000000000					
PP3         0.317         0.355         0.275         0.226         0.206         0.270         0.598         0.716         0.16         0.193         0.093         0.303           P11         0.411         0.463         0.368         0.288         0.343         0.328         0.261         0.445         0.876         0.121         -0.330         0.488           P12         0.306         0.251         0.230         0.342         0.307         0.273         0.188         0.428         0.898         -0.092         0.451         0.461         0.486           RTAA2         -0.139         -0.154         -0.159         0.081         -0.130         0.115         0.224         0.203         -0.066         0.866         0.354         0.044           RTAA3         -0.100         -0.153         -0.027         -0.008         -0.084         0.168         0.341         0.275         0.050         0.781         0.352         0.127           RTAA4         -0.016         0.017         -0.088         -0.084         0.169         0.131         0.155         0.337         0.215         0.050         0.073           RTAC1         -0.176         -0.127         -0.134         -0.027							2 2000		recognistic and the second				
P11									N. PO4600111100000000000000				
P12										content of any acceptance of the content of the con			
RTAA1         -0.032         0.104         -0.030         0.190         -0.118         0.212         0.192         0.227         0.073         0.632         0.061         0.186           RTAA2         -0.139         -0.154         -0.159         0.081         -0.130         0.115         0.234         0.023         -0.086         0.866         0.856         0.354         0.044           RTAA3         -0.010         -0.153         -0.024         0.088         -0.084         0.168         0.341         0.275         0.050         0.781         0.352         0.129           RTAC1         -0.016         -0.0134         -0.027         -0.088         0.010         0.235         0.185         -0.166         0.922         0.450         0.001           RTAC2         -0.222         -0.201         -0.058         0.010         -0.217         0.087         0.188         0.184         -0.097         0.857         0.455         0.001           RTAC3         -0.222         -0.201         -0.015         -0.250         0.060         0.214         0.184         -0.097         0.857         0.415         0.065           RTB1         0.191         0.191         0.050         0.224										0.0000760000000000000000000000000000000			
RTAA2         -0.139         -0.154         -0.159         0.081         -0.130         0.115         0.234         0.203         -0.086         0.866         0.354         0.044           RTAA3         -0.100         -0.153         -0.024         0.088         -0.084         0.168         0.341         0.275         0.050         0.781         0.352         0.129           RTAA4         -0.014         0.001         0.027         -0.088         -0.084         0.168         0.341         0.275         0.050         0.781         0.352         0.129           RTAC1         -0.176         -0.127         -0.134         -0.027         -0.168         0.100         0.235         0.185         -0.166         0.922         0.450         0.001           RTAC2         -0.222         -0.201         -0.058         0.010         -0.217         0.087         0.188         -0.184         -0.097         0.857         0.415         0.065           RTAC3         -0.228         -0.229         -0.169         0.015         0.060         0.214         0.184         -0.154         0.833         0.465         -0.015           RTBA         0.191         0.181         0.021         0.075										80	end-Services@CSDARS/Surji-		
RTAA3         -0.100         -0.153         -0.024         0.088         -0.084         0.168         0.341         0.275         0.050         0.781         0.352         0.129           RTAA4         -0.014         0.001         0.027         -0.008         -0.131         0.155         0.337         0.210         -0.207         0.435         0.073           RTAC1         -0.176         -0.127         -0.134         -0.027         -0.168         0.100         0.235         0.185         -0.166         0.922         0.450         0.000           RTAC2         -0.229         -0.201         -0.058         0.010         -0.217         0.087         0.188         0.184         -0.097         0.857         0.415         0.005           RTB1         0.191         0.181         0.021         0.074         0.315         0.165         0.346         0.207         0.009         0.222         0.333         0.465         -0.015           RTB1         0.191         0.181         0.021         0.074         0.315         0.165         0.346         0.207         0.009         0.222         0.333         0.465         0.015           RTB2         0.023         0.031         0.515<											SOUTH THE SECOND SECOND		
RTAA4         -0.014         0.001         0.027         -0.08         -0.131         0.155         0.337         0.210         -0.207         0.879         0.435         0.073           RTAC1         -0.176         -0.127         -0.134         -0.027         -0.168         0.100         0.235         0.185         -0.166         0.922         0.450         0.001           RTAC2         -0.222         -0.201         -0.058         0.010         -0.217         0.087         0.188         0.184         -0.097         0.857         0.415         0.065           RTAC3         -0.228         -0.229         -0.115         -0.250         0.060         0.214         0.184         -0.154         0.893         0.465         -0.015           RTB1         0.191         0.181         0.021         0.074         0.315         0.165         0.346         0.207         0.009         0.222         0.303         0.465         -0.015           RTB1         0.191         0.081         0.019         -0.099         0.271         0.148         -0.198         0.520         0.801         0.097           RTB2         0.003         0.0330         0.419         0.138         0.155         -0										9	2010/06/08/08/08/08		
RTAC1         -0.176         -0.127         -0.134         -0.027         -0.168         0.100         0.235         0.185         -0.166         0.922         0.450         0.001           RTAC2         -0.222         -0.201         -0.058         0.010         -0.217         0.087         0.188         0.184         -0.097         0.857         0.415         0.065           RTAC3         -0.228         -0.229         -0.169         -0.115         -0.250         0.060         0.214         0.184         -0.194         0.893         0.465         -0.018           RTB1         0.191         0.181         0.0201         0.074         0.315         0.165         0.346         0.207         -0.099         0.222         0.382         0.112           RTB2         0.023         -0.018         0.000         -0.160         0.019         -0.099         0.271         0.148         -0.198         0.520         0.801         0.097           RTB3         -0.085         -0.077         -0.026         -0.054         0.155         -0.078         0.125         0.208         -0.132         0.397         0.660         0.146           RTB4         0.104         0.129         0.023         <											1000 000 000000000000000000000000000000		
RTAC2         -0.222         -0.201         -0.058         0.010         -0.217         0.087         0.188         0.184         -0.097         0.857         0.415         0.065           RTAC3         -0.228         -0.229         -0.169         -0.115         -0.250         0.060         0.214         0.184         -0.154         0.893         0.465         -0.015           RTB1         0.191         0.181         0.021         0.074         0.315         0.165         0.346         0.207         0.009         0.222         0.382         0.112           RTB2         0.023         -0.018         0.000         -0.160         0.0155         -0.078         0.125         0.208         -0.132         0.337         0.600         0.146           RTB3         0.085         -0.077         -0.026         -0.054         0.155         -0.078         0.125         0.208         -0.132         0.337         0.600         0.146           RTB4         0.104         0.129         -0.035         -0.035         -0.0155         0.0186         0.314         0.273         0.125         0.361         0.362         0.045         0.257         0.376         0.330         0.441         0.362											000000000000000000000000000000000000000		
RTAC3         -0.228         -0.229         -0.169         -0.115         -0.250         0.060         0.214         0.184         -0.154         0.893         0.465         -0.015           RTB1         0.191         0.181         0.021         0.074         0.315         0.165         0.346         0.207         0.009         0.222         0.382         0.112           RTB2         0.023         -0.018         0.000         -0.160         0.019         -0.099         0.271         0.148         -0.198         0.520         0.801         0.097           RTB3         -0.085         -0.077         -0.026         -0.053         -0.023         0.155         -0.078         0.125         0.208         -0.132         0.339         0.680         0.146           RTB4         0.104         0.129         -0.035         -0.023         0.155         -0.078         0.125         0.203         -0.132         0.380         0.680         0.046           JS1         0.130         0.175         0.004         0.233         0.194         0.193         0.203         0.348         0.236         0.227         0.078         0.419           JS2         0.135         0.041         0.549 <th></th>													
RTB1         0.191         0.181         0.021         0.074         0.315         0.165         0.346         0.207         0.009         0.222         0.382         0.112           RTB2         0.023         -0.018         0.000         -0.160         0.019         -0.099         0.271         0.148         -0.198         0.520         0.801         0.097           RTB3         -0.085         -0.077         -0.026         -0.054         0.155         -0.078         0.125         0.208         -0.132         0.997         0.680         0.146           RTB4         0.104         0.129         -0.035         -0.023         0.155         -0.078         0.314         0.273         -0.122         0.382         0.680         0.073           JS1         0.330         0.339         0.372         0.357         0.257         0.376         0.303         0.441         0.367         0.238         0.619           JS2         0.190         0.175         0.004         0.233         0.194         0.193         0.203         0.348         0.236         0.227         0.078         0.419           JS3         0.478         0.429         0.286         0.462         0.316											0.893	0.465	-0.015
RTB2         0.023         -0.018         0.000         -0.160         0.019         -0.099         0.271         0.148         -0.198         0.520         0.801         0.097           RTB3         -0.085         -0.077         -0.026         -0.054         0.155         -0.078         0.125         0.208         -0.132         0.397         0.680         0.146           RTB4         0.104         0.129         -0.035         -0.023         0.153         -0.018         0.314         0.273         -0.122         0.382         0.680         0.073           JS1         0.330         0.339         0.372         0.357         0.257         0.376         0.303         0.441         0.367         0.236         -0.138         0.619           JS3         0.478         0.427         0.341         0.549         0.346         0.528         0.156         0.364         0.377         -0.007         -0.164         0.736           JS4         0.295         0.337         0.172         0.429         0.286         0.452         0.156         0.364         0.377         -0.007         -0.164         0.736           JS5         0.361         0.361         0.308         0.450							0.165	0.346	0.207	0.009	0.222	0.382	0.112
RTB3         -0.085         -0.077         -0.026         -0.054         0.155         -0.078         0.125         0.208         -0.132         0.397         0.680         0.146           RTB4         0.104         0.129         -0.035         -0.023         0.153         -0.018         0.314         0.273         -0.122         0.382         0.680         0.073           JS1         0.330         0.339         0.372         0.357         0.257         0.376         0.303         0.441         0.367         0.236         -0.138         0.619           JS3         0.478         0.427         0.341         0.549         0.346         0.528         0.156         0.364         0.377         -0.007         -0.164         0.736           JS4         0.295         0.337         0.172         0.429         0.286         0.462         0.316         0.401         0.288         0.159         -0.045         0.725           JS5         0.361         0.361         0.308         0.450         0.451         0.490         0.278         0.404         0.344         0.158         0.175         0.0736           JS6         0.298         0.287         0.303         0.270         <				0.000	-0.160	0.019	-0.099	0.271	0.148	-0.198	0.520	0.801	0.097
151   0.330   0.339   0.372   0.357   0.257   0.376   0.303   0.441   0.367   0.236   -0.138   0.619     152   0.190   0.175   0.004   0.233   0.194   0.193   0.203   0.348   0.236   0.227   0.078   0.419     153   0.478   0.427   0.341   0.549   0.346   0.528   0.156   0.364   0.377   -0.007   -0.164   0.736     154   0.295   0.337   0.172   0.429   0.286   0.462   0.316   0.401   0.288   0.159   -0.045   0.725     155   0.361   0.361   0.308   0.450   0.451   0.490   0.278   0.404   0.344   0.158   -0.175   0.736     156   0.298   0.287   0.303   0.270   0.301   0.300   0.165   0.308   0.349   0.071   -0.158   0.638     157   0.464   0.442   0.434   0.436   0.449   0.503   0.308   0.423   0.418   0.073   -0.161   0.817     158   0.522   0.400   0.369   0.454   0.340   0.543   0.270   0.267   0.288   0.077   -0.171   0.752     159   0.501   0.410   0.466   0.554   0.502   0.552   0.187   0.376   0.463   0.048   -0.272   0.844     1510   0.471   0.353   0.336   0.534   0.474   0.513   0.225   0.341   0.353   0.086   -0.197   0.827     1511   0.447   0.382   0.415   0.545   0.477   0.534   0.168   0.348   0.506   -0.006   -0.255   0.818     1512   0.536   0.492   0.485   0.477   0.485   0.558   0.278   0.437   0.458   -0.078   -0.239   0.818     1513   0.407   0.411   0.383   0.459   0.434   0.521   0.202   0.453   0.357   0.064   -0.183   0.826     1514   0.437   0.353   0.279   0.521   0.401   0.453   0.244   0.422   0.446   -0.013   -0.228   0.748     1515   0.417   0.341   0.209   0.440   0.404   0.448   0.261   0.302   0.348   0.079   -0.178   0.731     1516   0.477   0.387   0.319   0.506   0.417   0.472   0.143   0.336   0.366   0.058   -0.199   0.726     1517   0.418   0.367   0.406   0.550   0.455   0.520   0.507   0.184   0.378   0.452   -0.039   -0.306   0.858     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1519   0.402   0.336   0.32		-0.085	-0.077	-0.026	-0.054	0.155	-0.078	0.125	0.208	-0.132	0.397	0.680	0.146
152   0.190   0.175   0.004   0.233   0.194   0.193   0.203   0.348   0.236   0.227   0.078   0.419     153   0.478   0.427   0.341   0.549   0.346   0.528   0.156   0.364   0.377   -0.007   -0.164   0.736     154   0.295   0.337   0.172   0.429   0.286   0.462   0.316   0.401   0.288   0.159   -0.045     155   0.361   0.361   0.308   0.450   0.451   0.490   0.278   0.404   0.344   0.158   -0.175   0.736     156   0.298   0.287   0.303   0.270   0.301   0.300   0.165   0.308   0.349   0.071   -0.158   0.638     157   0.464   0.442   0.434   0.436   0.449   0.503   0.308   0.423   0.418   0.073   -0.161   0.817     158   0.522   0.400   0.369   0.454   0.340   0.543   0.270   0.267   0.288   0.077   -0.171   0.752     159   0.501   0.410   0.466   0.554   0.502   0.552   0.187   0.376   0.463   0.048   -0.272   0.844     1510   0.471   0.353   0.336   0.534   0.474   0.513   0.225   0.341   0.353   0.086   -0.197   0.827     1511   0.447   0.382   0.415   0.545   0.477   0.534   0.168   0.348   0.506   -0.006   -0.255   0.818     1512   0.536   0.492   0.485   0.477   0.485   0.558   0.278   0.437   0.458   -0.078   -0.239   0.818     1513   0.407   0.411   0.383   0.459   0.434   0.521   0.202   0.453   0.357   0.064   -0.183   0.826     1514   0.437   0.353   0.279   0.521   0.401   0.453   0.244   0.422   0.446   -0.013   -0.228   0.748     1515   0.417   0.341   0.209   0.440   0.404   0.448   0.261   0.302   0.348   0.079   -0.178   0.731     1516   0.477   0.387   0.319   0.506   0.417   0.472   0.143   0.336   0.366   0.058   -0.199   0.726     1517   0.418   0.367   0.406   0.550   0.455   0.548   0.236   0.472   0.470   0.074   -0.230   0.905     1518   0.432   0.352   0.424   0.545   0.520   0.507   0.184   0.378   0.452   -0.039   -0.306   0.858     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.150   0.367   0.412   0.066   -0.222   0.815     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1519   0.402   0.336   0.321   0.5	RTB4	0.104	0.129	-0.035	-0.023	0.153	-0.018	0.314	0.273	-0.122	0.382	0.680	nuclei, han exception to an understanding or
153	JS1	0.330	0.339	0.372	0.357			0.303				- 2	COLORO PROGRAMMO PROGRAMMO
154   0.295   0.337   0.172   0.429   0.286   0.462   0.316   0.401   0.288   0.159   -0.045   0.725     155   0.361   0.361   0.308   0.450   0.451   0.490   0.278   0.404   0.344   0.158   -0.175   0.736     156   0.298   0.287   0.303   0.270   0.301   0.300   0.165   0.308   0.349   0.071   -0.158   0.638     157   0.464   0.442   0.434   0.436   0.449   0.503   0.308   0.423   0.418   0.073   -0.161   0.817     158   0.522   0.400   0.369   0.454   0.340   0.543   0.270   0.267   0.288   0.077   -0.171   0.752     159   0.501   0.410   0.466   0.554   0.502   0.552   0.187   0.376   0.463   0.048   -0.272   0.844     1510   0.471   0.353   0.336   0.534   0.474   0.513   0.225   0.341   0.353   0.086   -0.197   0.827     1511   0.447   0.382   0.415   0.545   0.477   0.534   0.168   0.348   0.506   -0.006   -0.255   0.818     1512   0.536   0.492   0.485   0.477   0.485   0.558   0.278   0.437   0.458   -0.078   -0.239   0.818     1513   0.407   0.411   0.383   0.459   0.434   0.521   0.202   0.453   0.357   0.064   -0.183   0.826     1514   0.437   0.353   0.279   0.521   0.401   0.453   0.244   0.422   0.446   -0.013   -0.228   0.748     1515   0.417   0.341   0.209   0.440   0.404   0.448   0.261   0.302   0.348   0.079   -0.178   0.731     1516   0.477   0.387   0.319   0.506   0.417   0.472   0.143   0.336   0.366   0.058   -0.199   0.726     1517   0.418   0.367   0.406   0.550   0.455   0.548   0.236   0.472   0.470   0.074   -0.230   0.905     1518   0.432   0.352   0.424   0.545   0.520   0.507   0.184   0.378   0.452   -0.039   -0.306   0.858     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1519   0.402   0.336   0.321   0	JS2											8	
155   0.361   0.361   0.308   0.450   0.451   0.490   0.278   0.404   0.344   0.158   -0.175   0.736     156   0.298   0.287   0.303   0.270   0.301   0.300   0.165   0.308   0.349   0.071   -0.158   0.638     157   0.464   0.442   0.434   0.436   0.449   0.503   0.308   0.423   0.418   0.073   -0.161   0.817     158   0.522   0.400   0.369   0.454   0.340   0.543   0.270   0.267   0.288   0.077   -0.171   0.752     159   0.501   0.410   0.466   0.554   0.502   0.552   0.187   0.376   0.463   0.048   -0.272   0.844     1510   0.471   0.353   0.336   0.534   0.474   0.513   0.225   0.341   0.353   0.086   -0.197   0.827     1511   0.447   0.382   0.415   0.545   0.477   0.534   0.168   0.348   0.506   -0.006   -0.255   0.818     1512   0.536   0.492   0.485   0.477   0.485   0.558   0.278   0.437   0.458   -0.078   -0.239   0.818     1513   0.407   0.411   0.383   0.459   0.434   0.521   0.202   0.453   0.357   0.064   -0.183   0.826     1514   0.437   0.353   0.279   0.521   0.401   0.453   0.244   0.422   0.446   -0.013   -0.228   0.748     1515   0.417   0.341   0.209   0.440   0.404   0.448   0.261   0.302   0.348   0.079   -0.178   0.731     1516   0.477   0.387   0.319   0.506   0.417   0.472   0.143   0.336   0.366   0.058   -0.199   0.726     1517   0.418   0.367   0.406   0.550   0.455   0.548   0.236   0.472   0.470   0.074   -0.230   0.905     1518   0.432   0.352   0.424   0.545   0.520   0.507   0.184   0.378   0.452   -0.039   -0.306   0.858     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1510   0.402   0.336   0.321													
156   0.298   0.287   0.303   0.270   0.301   0.300   0.165   0.308   0.349   0.071   -0.158   0.638     157	JS4											1	
157   0.464   0.442   0.434   0.436   0.449   0.503   0.308   0.423   0.418   0.073   -0.161   0.817     158   0.522   0.400   0.369   0.454   0.340   0.543   0.270   0.267   0.288   0.077   -0.171   0.752     159   0.501   0.410   0.466   0.554   0.502   0.552   0.187   0.376   0.463   0.048   -0.272   0.844     1510   0.471   0.353   0.336   0.534   0.474   0.513   0.225   0.341   0.353   0.086   -0.197   0.827     1511   0.447   0.382   0.415   0.545   0.477   0.534   0.168   0.348   0.506   -0.006   -0.255   0.818     1512   0.536   0.492   0.485   0.477   0.485   0.558   0.278   0.437   0.458   -0.078   -0.239   0.818     1513   0.407   0.411   0.383   0.459   0.434   0.521   0.202   0.453   0.357   0.064   -0.183   0.826     1514   0.437   0.353   0.279   0.521   0.401   0.453   0.244   0.422   0.446   -0.013   -0.228   0.748     1515   0.417   0.341   0.209   0.440   0.404   0.448   0.261   0.302   0.348   0.079   -0.178   0.731     1516   0.477   0.387   0.319   0.506   0.417   0.472   0.143   0.336   0.366   0.058   -0.199   0.726     1517   0.418   0.367   0.406   0.550   0.455   0.548   0.236   0.472   0.470   0.074   -0.230   0.905     1518   0.432   0.352   0.424   0.545   0.520   0.507   0.184   0.378   0.452   -0.039   -0.306   0.858     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1510   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1511   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1512   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1513   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1514   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1515   0.402   0.402   0.402													
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159   0.501   0.410   0.466   0.554   0.502   0.552   0.187   0.376   0.463   0.048   -0.272   0.844     1510   0.471   0.353   0.336   0.534   0.474   0.513   0.225   0.341   0.353   0.086   -0.197   0.827     1511   0.447   0.382   0.415   0.545   0.477   0.534   0.168   0.348   0.506   -0.006   -0.255   0.818     1512   0.536   0.492   0.485   0.477   0.485   0.558   0.278   0.437   0.458   -0.078   -0.239   0.818     1513   0.407   0.411   0.383   0.459   0.434   0.521   0.202   0.453   0.357   0.064   -0.183   0.826     1514   0.437   0.353   0.279   0.521   0.401   0.453   0.244   0.422   0.446   -0.013   -0.228   0.748     1515   0.417   0.341   0.209   0.440   0.404   0.448   0.261   0.302   0.348   0.079   -0.178   0.731     1516   0.477   0.387   0.319   0.506   0.417   0.472   0.143   0.336   0.366   0.058   -0.199   0.726     1517   0.418   0.367   0.406   0.550   0.455   0.548   0.236   0.472   0.470   0.074   -0.230   0.905     1518   0.432   0.352   0.424   0.545   0.520   0.507   0.184   0.378   0.452   -0.039   -0.306   0.858     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1510   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1510   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1511   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1512   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1513   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1514   0.407   0.408												9	55.000 98.000 0000000000000000000000000000
S10												- 1	1000-000 CENTROLOGICA (CONTROL
JS11         0.447         0.382         0.415         0.545         0.477         0.534         0.168         0.348         0.506         -0.006         -0.255         0.818           JS12         0.536         0.492         0.485         0.477         0.485         0.558         0.278         0.437         0.458         -0.078         -0.239         0.818           JS13         0.407         0.411         0.383         0.459         0.434         0.521         0.202         0.453         0.357         0.064         -0.183         0.826           JS14         0.437         0.353         0.279         0.521         0.401         0.453         0.244         0.422         0.446         -0.013         -0.228         0.748           JS15         0.417         0.341         0.209         0.440         0.404         0.448         0.261         0.302         0.348         0.079         -0.178         0.731           JS16         0.477         0.387         0.319         0.506         0.417         0.472         0.143         0.336         0.366         0.058         -0.199         0.726           JS17         0.418         0.367         0.406         0.550 <t< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></t<>													
1512   0.536   0.492   0.485   0.477   0.485   0.558   0.278   0.437   0.458   -0.078   -0.239   0.818     1513   0.407   0.411   0.383   0.459   0.434   0.521   0.202   0.453   0.357   0.064   -0.183   0.826     1514   0.437   0.353   0.279   0.521   0.401   0.453   0.244   0.422   0.446   -0.013   -0.228   0.748     1515   0.417   0.341   0.209   0.440   0.404   0.448   0.261   0.302   0.348   0.079   -0.178   0.731     1516   0.477   0.387   0.319   0.506   0.417   0.472   0.143   0.336   0.366   0.058   -0.199   0.726     1517   0.418   0.367   0.406   0.550   0.455   0.548   0.236   0.472   0.470   0.074   -0.230   0.905     1518   0.432   0.352   0.424   0.545   0.520   0.507   0.184   0.378   0.452   -0.039   -0.306   0.858     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1519   0.402   0.336   0.321   0.515   0.445   0.449   0.150   0.367   0.412   0.066   -0.222   0.815     1510   0.407   0.408   0.408   0.409   0.150   0.367   0.412   0.066   -0.222   0.815     1510   0.408   0.408   0.408   0.408   0.409   0.150   0.367   0.412   0.066   -0.222   0.815     1510   0.408   0.408   0.408   0.408   0.409   0.150   0.367   0.412   0.066   -0.222   0.815     1511   0.408   0.												3	CONTRACTOR OF THE PROPERTY OF
JS13         0.407         0.411         0.383         0.459         0.434         0.521         0.202         0.453         0.357         0.064         -0.183         0.826           JS14         0.437         0.353         0.279         0.521         0.401         0.453         0.244         0.422         0.446         -0.013         -0.228         0.748           JS15         0.417         0.341         0.209         0.440         0.404         0.448         0.261         0.302         0.348         0.079         -0.178         0.731           JS16         0.477         0.387         0.319         0.506         0.417         0.472         0.143         0.336         0.356         0.058         -0.199         0.726           JS17         0.418         0.367         0.406         0.550         0.455         0.548         0.236         0.472         0.470         0.074         -0.230         0.905           JS18         0.432         0.352         0.424         0.545         0.520         0.507         0.184         0.378         0.452         -0.039         -0.306         0.858           JS19         0.402         0.336         0.321         0.515 <th< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>8</th><th></th></th<>												8	
JS14         0.437         0.353         0.279         0.521         0.401         0.453         0.244         0.422         0.446         -0.013         -0.228         0.748           JS15         0.417         0.341         0.209         0.440         0.404         0.448         0.261         0.302         0.348         0.079         -0.178         0.731           JS16         0.477         0.387         0.319         0.506         0.417         0.472         0.143         0.336         0.366         0.058         -0.199         0.726           JS17         0.418         0.367         0.406         0.550         0.455         0.548         0.236         0.472         0.470         0.074         -0.230         0.905           JS18         0.432         0.352         0.424         0.545         0.520         0.507         0.184         0.378         0.452         -0.039         -0.306         0.858           JS19         0.402         0.336         0.321         0.515         0.445         0.449         0.150         0.367         0.412         0.066         -0.222         0.815												9	100000000000000000000000000000000000000
JS15         0.417         0.341         0.209         0.440         0.404         0.448         0.261         0.302         0.348         0.079         -0.178         0.731           JS16         0.477         0.387         0.319         0.506         0.417         0.472         0.143         0.336         0.366         0.058         -0.199         0.726           JS17         0.418         0.367         0.406         0.550         0.455         0.548         0.236         0.472         0.470         0.074         -0.230         0.905           JS18         0.432         0.352         0.424         0.545         0.520         0.507         0.184         0.378         0.452         -0.039         -0.306         0.858           JS19         0.402         0.336         0.321         0.515         0.445         0.449         0.150         0.367         0.412         0.066         -0.222         0.815													CONTROL OF THE PROPERTY OF THE
JS16         0.477         0.387         0.319         0.506         0.417         0.472         0.143         0.336         0.366         0.058         -0.199         0.726           JS17         0.418         0.367         0.406         0.550         0.455         0.548         0.236         0.472         0.470         0.074         -0.230         0.905           JS18         0.432         0.352         0.424         0.545         0.520         0.507         0.184         0.378         0.452         -0.039         -0.306         0.858           JS19         0.402         0.336         0.321         0.515         0.445         0.449         0.150         0.367         0.412         0.066         -0.222         0.815												*	CONTRACTOR STATE OF THE PARTY O
JS17         0.418         0.367         0.406         0.550         0.455         0.548         0.236         0.472         0.470         0.074         -0.230         0.905           JS18         0.432         0.352         0.424         0.545         0.520         0.507         0.184         0.378         0.452         -0.039         -0.306         0.858           JS19         0.402         0.336         0.321         0.515         0.445         0.449         0.150         0.367         0.412         0.066         -0.222         0.815													
JS18         0.432         0.352         0.424         0.545         0.520         0.507         0.184         0.378         0.452         -0.039         -0.306         0.858           JS19         0.402         0.336         0.321         0.515         0.445         0.449         0.150         0.367         0.412         0.066         -0.222         0.815												1	CECURE CONTRACTOR SERVICES
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	JS20	0.471									0.021		0.898

A summary of the latent mean of all constructs is shown in Table 26. More details of the mean comparison are furnished in Appendix B.

Table 26 Descriptive statistics of the three cases

Construct Group	Acronym	POSTAL	ENERGY	WATER
		(N = 107)	(N=483)	(N=100)
User Acceptance	PU	3.48	3.27	3.44
	PEU	3.15	2.93	2.97
	SN	3.15	3.01	3.03
	ATU	3.57	3.40	3.53
	IU	3.36	3.34	3.20
	SA	3.43	3.29	3.27
User Resistance	PSE	3.40	3.01	2.97
	PP	2.67	2.61	2.37
	PI	3.05	3.00	2.74
	RTA	2.42	2.37	2.21
	RTB	2.55	2.53	2.27
Job-related Outcomes	JS	3.26	3.05	3.21

#### 4.4 Empirical Assessment of Theoretical Models

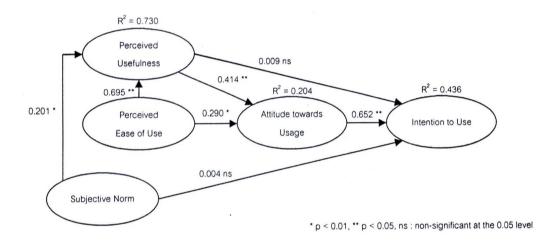
This section illustrates the results of the empirical assessment of the theoretical models pertinent to the research questions of this study: TAM, Resistance to Change, and the proposed model. Theoretical models were tested with data obtained from the three cases. A PLS approach to SEM with bootstrap sub-sampling (n = 1,000) was employed. First, two versions of TAM conceptualized with two different dependent variables were tested, namely, system usage and symbolic adoption. This was to examine the extent to which antecedents in TAM could predict symbolic adoption in mandatory-use context. Second, models with constructs derived from the resistance to change theories were tested. Lastly, the proposed models were empirically assessed.

#### 4.4.1 Empirical Assessment of Technology Acceptance Model

To broadly examine how users react with a mandatory-use system, TAM with SN and ATU included was tested with data from the three organizations. This was to show the general application of the use of TAM in this particular setting. Even though the relationship between an intention to use and its determinants is statistically significant, TAM still offers limited explanations to the question related to user acceptance, as discussed in the previous chapters.

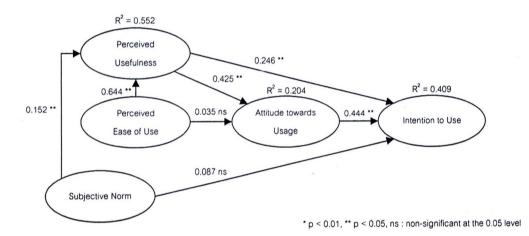
#### Postal

Most hypothesized paths were statistically significant at 0.01 level. ATU, one out of three, was found to be a statistically significant antecedent of IU (t=5.716, p<0.01). On the one hand, the other two antecedents with no statistical significant relationship were antecedents that were PU and SN (t=0.101, p>0.05 and t=0.072, p>0.05). These three constructs jointly explained the 43.6% of variance in Intention to use. Both PU and PEU were found to be a statistically significant determinant of ATU and explained 20.4% of the variance.



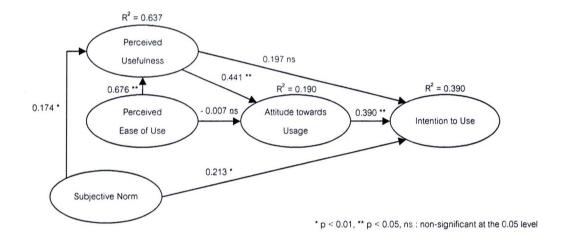
### Energy

The results show that there were only two paths found not to be statistically significant: the path from PEU to ATU (t=0.694, p>0.05) and the other path from SN to IU (t=1.734, p>0.05). Other hypothesized relationships were statistically significant at 0.01 level. The 20.4% of the variance in ATU was explained by PEU and PU. ATU was a significant antecedent of IU (t=5.677, p<0.01) and together with SN explained 40.9% of the variance in IU.



#### Water

The results of this empirical assessment in the case of WATER are somewhat different from the results of the previous two cases. ATU and SN appear to be a primary significant determinant of IU (t=2.685, p<0.01 and t=2.079, p<0.05). PU were not found to be a statistically significant antecedent of IU (t=1.339, p>0.05). The path from SN to PU was statistically significant (t=1.966, p<0.05). The variance in IU was explained by three theoretical constructs, about 39.0%. The 19.0% of variance in ATU was explained by PU and PEU.



### 4.4 Empirical Assessment of Theoretical Models

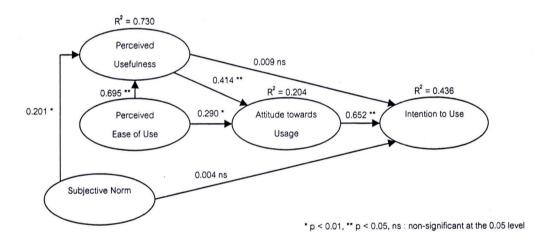
This section illustrates the results of the empirical assessment of the theoretical models pertinent to the research questions of this study: TAM, Resistance to Change, and the proposed model. Theoretical models were tested with data obtained from the three cases. A PLS approach to SEM with bootstrap sub-sampling (n = 1,000) was employed. First, two versions of TAM conceptualized with two different dependent variables were tested, namely, system usage and symbolic adoption. This was to examine the extent to which antecedents in TAM could predict symbolic adoption in mandatory-use context. Second, models with constructs derived from the resistance to change theories were tested. Lastly, the proposed models were empirically assessed.

#### 4.4.1 Empirical Assessment of Technology Acceptance Model

To broadly examine how users react with a mandatory-use system, TAM with SN and ATU included was tested with data from the three organizations. This was to show the general application of the use of TAM in this particular setting. Even though the relationship between an intention to use and its determinants is statistically significant, TAM still offers limited explanations to the question related to user acceptance, as discussed in the previous chapters.

#### Postal

Most hypothesized paths were statistically significant at 0.01 level. ATU, one out of three, was found to be a statistically significant antecedent of IU (t = 5.716, p < 0.01). On the one hand, the other two antecedents with no statistical significant relationship were antecedents that were PU and SN (t = 0.101, p > 0.05 and t = 0.072, p > 0.05). These three constructs jointly explained the 43.6% of variance in Intention to use. Both PU and PEU were found to be a statistically significant determinant of ATU and explained 20.4% of the variance.

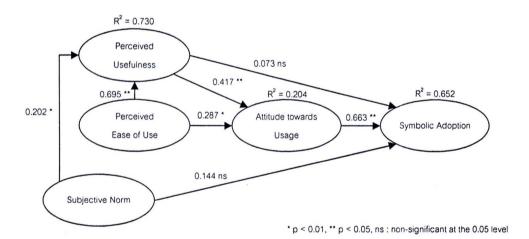


# 4.4.2 Empirical Assessment of Technology Acceptance Model with Symbolic Adoption as a Dependent Variable

As the literature suggests, SA should be placed as a dependent variable when the usage is mandatory. Some researchers have shown that PU, PEU and ATU are significant determinants of SA (Nah et al., 2004). Following TAM conceptualization, these sub-models would be empirically assessed to explore to what extent TAM original determinants could predict SA. PU, PEU, and SN were hypothesized to predict a level of SA in the mandatory-usage setting.

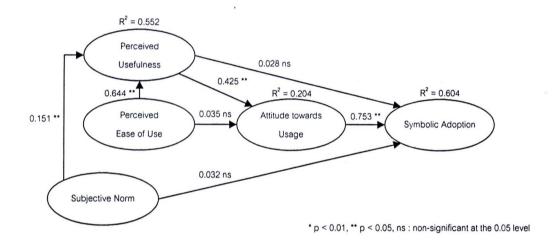
#### Postal

Most hypothesized relationships were statistically significant at 0.01 level. Two out of three theorized determinants were not found to be a statistical significant determinant. SN was not found to be statistically significantly related with SA (t = 1.323, p > 0.05). The relationship between PU and SA was not statistically significant (t = 0.711, p > 0.05). This left ATU to be the only statistical significant determinant of SA (t = 5.749, p < 0.01). The three constructs, PU, ATU, and SN, jointly explained the 65.2% of variance in SA. The 20.4% variance of ATU were both explained and determined by PU and PEU (t = 3.438, p < 0.01 and t = 2.302, p > 0.05).



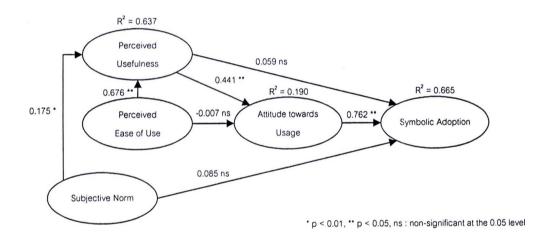
#### Energy

Most hypothesized relationships were statistically significant at 0.01 level. Three paths were not found to be statistically significant. These include paths from PEU to ATU (t = 0.685, p > 0.05), from PU to SA (t = 0.832, p > 0.05), and from SN to SA (t = 1.039, p > 0.05). The relationship between ATU and SA appears to be relatively high (b = 0.753, p < 0.01). The 60.44% of the variance in SA was explained by PU, ATU, and SN.



#### Water

The results obtained from the case of WATER are quite uncommon. There were only two statistically significant paths: the path from PEU to PU (t = 6.617, p < 0.01) and the path from ATU to SA (t = 6.231, p < 0.01). Apart from ATU, the other two theorized determinants, PU and SN, were not statistically significantly related with SA (t = 0.740, p > 0.05 and t = 1.211, p > 0.05, respectively). These three constructs together explained 68.1% of the variance in SA. In addition, ATU was not statistically significantly related with the two hypothesized antecedents; PU and PEU (t = 1.927, p > 0.05 and t = 0.222, p > 0.05, correspondingly).



that SN was not significantly related to IU, the effect of this social influence is most likely to enhance the level of PU.

In summary, the findings seem to confirm most of the results found in previous studies. Perceived usefulness is the primary determinant of an intention to use mediated by attitude towards the system usage. Since users might feel that ERP was quite difficult to operate, perceived ease of use did not directly influence attitude towards system usage but helped to improve the perception of usefulness.

Table 27 Summary of structural model path coefficients and explained variance of the empirical assessment of technology acceptance model

	Structu	ral model path coef	ficients
	POSTAL	ENERGY	WATER
PEU → PU	0.695 **	0.644 **	0.676 **
SN → PU	0.201 *	0.152 **	0.174 *
PEU → ATU	0.290 *	0.035 ns	-0.007 ns
PU → ATU	0.414 **	0.425 **	0.441 **
PU → IU	0.009 ns	0.246 **	0.197 ns
ATU → IU	0.652 **	0.444 **	0.390 **
SN → IU	0.004 ns	0.087 ns	0.213 *
Variance explained in PU	73.0%	55.2%	63.7%
Variance explained in ATU	20.4%	24.6%	19.0%
Variance explained in IU	43.6%	40.9%	39.0%

Table 28 Summary of structural model path coefficients and explained variance of the empirical assessment of technology acceptance model with symbolic adoption as a dependent variable

	Structu	ral model path coef	ficients
	POSTAL	ENERGY	WATER
PEU → PU	0.695 **	0.644 **	0.676 **
SN → PU	0.202 *	0.151 **	0.175 *
PEU → ATU	0.287 *	0.035 ns	-0.007 ns
PU → ATU	0.417 **	0.425 **	0.441 **
PU → SA	0.073 ns	0.028 ns	0.076 ns
ATU → SA	0.663 **	0.753 **	0.762 **
SN → SA	0.144 ns	0.032 ns	0.085 ns
Variance explained in PU	73.0%	55.2%	63.7%
Variance explained in ATU	20.4%	20.4%	19.0%
Variance explained in SA	65.2%	60.4%	66.5%

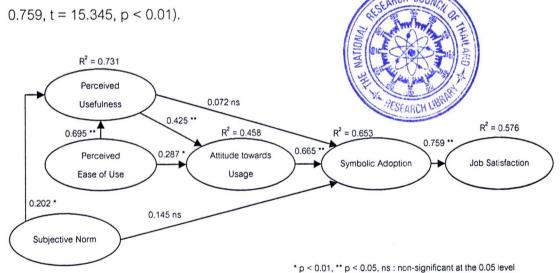


# 4.4.3 Empirical Assessment of Technology Acceptance Model with Symbolic Adoption predicting Job-Related Outcomes Variable

To address one of the research questions in this study: To what extent are job-related outcomes affected by user acceptance and user resistance in a mandatory-use context? The sub-models of TAM with SA predicting job-related outcomes were tested to examine the relationship between user acceptance and job-related outcomes.

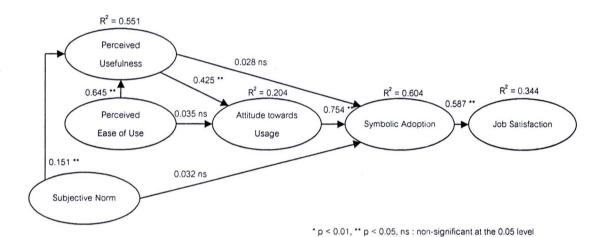
#### Postal

There are two hypothesized paths that were not found to be statistically significant at 0.05 level. PU was not statistically positively significantly related to SA (t = 0.771, p > 0.05). And the relationship between SN and SA was not statistically significant (t = 1.522, p > 0.05). Thus, ATU was the primary determinant of SA (b = 0.665, t = 7.838, p < 0.01). The variance of SA was explained by the three variables, about 65.3%. The results suggest that SA was relatively highly related with JS (b =  $\frac{1}{1000}$ ).



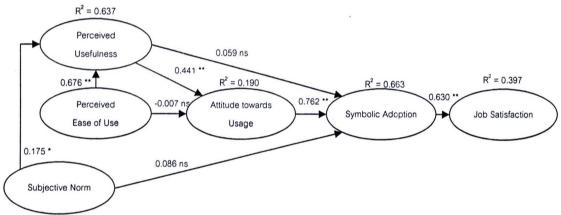
# Energy

When symbolic adoption was hypothesized to have a positive direct effect on job satisfaction, the results show that both hypothesized paths were statistically significant (t = 8.760, p < 0.01). ATU seems to be a relatively strong determinant of SA (b = 0.754, t = 14.204, p < 0.01), while PU and SN were not statistically significantly related with SA (t = 0.641, p > 0.05 and t = 0.811, p > 0.05, respectively). ATU, PU, and SN together explained 60.4% of the variance in SA.



#### Water

The results suggest that ATU was a major determinant of SA. ATU is relatively highly correlated with SA at 0.01 statistically significant (b = 0.762, t = 6.635, p < 0.01), whereas the other two hypothesized determinants, PU and SN, were not found to be statistically significantly related with SA (t = 0.417, p > 0.05 and t = 1.238, p > 0.05, respectively). The 66.3% variance of SA was jointly explained by ATU, PU, and SN. Furthermore, SA was statistically significantly related with JS (t = 7.649, p < 0.01).



\* p < 0.01, \*\* p < 0.05, ns : non-significant at the 0.05 level

Summary of the Empirical Assessment of Technology Acceptance Model with Symbolic Adoption predicting Job-Related Outcomes

Table 29 presents path coefficients, explained variance, and statistical significance from the three structural models. When SA is conceptualized to predict job-related outcomes, the evidence from the three cases suggests that SA could significantly predict JS. The relationships between SA and JS are moderately high (the path coefficients range from 0.63 to 0.76, approximately). It is probable that an individual with a more positive attitude towards usage will have a higher degree of symbolic adoption. They will be more accepting of the idea of adopting this particular technology. With a high level of symbolic adoption, an individual will have high job satisfaction.

Table 29 Summary of structural model path coefficients and explained variance of the empirical assessment of technology acceptance model with symbolic adoption as a dependent variable predicting job-related outcomes

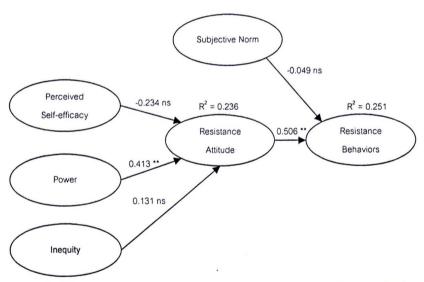
	Structural model path coefficients		
	POSTAL	ENERGY	WATER
PEU → PU	0.695 **	0.645 **	0.676 *
SN → PU	0.202 *	0.151 **	0.175 *
PEU → ATU	0.287 *	0.035 ns	-0.007 ns
PU → ATU	0.425 **	0.425 **	0.441 *
PU → SA	0.072 ns	0.028 ns	0.059 ns
ATU → SA	0.665 **	0.754 **	0.762 **
SN → SA	0.145 ns	0.032 ns	0.085 ns
SA → JS	0.759 **	0.587 **	0.630 **
Variance explained in PU	73.1%	55.1%	63.7%
Variance explained in ATU	45.8%	20.4%	19.0%
Variance explained in SA	65.3%	60.4%	66.3%
Variance explained in JS	57.6%	34.4%	39.7%

# 4.4.4 Empirical Assessment of Resistance to IS implementation Model

Resistance to IS implementation sub-models was empirically assessed in order to examine what could potentially influence resistance to IS implementation. PSE, PP, and PI were hypothesized to influence resistance attitude which, in turn, jointly determine resistance behaviors with SN.

#### Postal

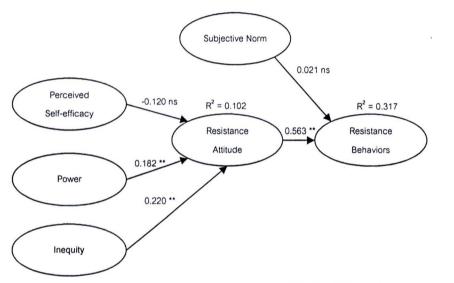
Only PP was statistically significantly related to RTA (t = 4.234, p < 0.01), whereas, PSE and PI were not a statistically significant determinant of RTA (t = 1.915, p > 0.05 and t = 1.165, p > 0.05, correspondingly). These three constructs jointly explained 23.6% variance in RTA. The relationship between RTA and RTB was statistically significant (t = 5.431, p < 0.01). However, SN was not found to be statistically significantly related to RTB (t = 0.376, p > 0.05). The 25.1% of variance in RTB was explained by RTA and SN.



\* p < 0.01, \*\* p < 0.05, ns : non-significant at the 0.05 level

## **ENERGY**

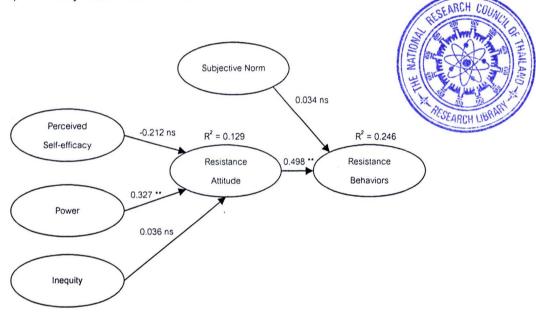
Two of three hypothesized antecedents of RTA were found to be statistically significant; PP and PI. The relationship between PSE and RTA was not statistically significant (t = 1.370, p > 0.05). These three antecedents jointly explained 10.2% of variance in RTA. The variance explained seems to be somewhat low. RTB were significantly related to only RTA (t = 12.075, p < 0.01). SN was not found to significantly influent RTB (t = 0.401, p > 0.05).



\* p < 0.01, \*\* p < 0.05, ns : non-significant at the 0.05 level

#### WATER

Two of the three hypothesized determinants of RTA were not found to be statistically significant (t = 1.191, p > 0.05 and t = 0.261, p > 0.05 for PSE and PI, respectively). PP was significantly related to RTA (t = 2.850, p < 0.01). There were two hypothesized antecedents of RTB: RTA and SN. RTA was moderately correlated with RTB at 0.01 statistical significant level (t = 5.381, p < 0.01), while SN was not statistically significantly related to RTB (t = 0.373, p > 0.05). 24.6% of the variance in RTB was explained by these two constructs.



 $^{\star}$  p < 0.01,  $^{\star\star}$  p < 0.05, ns : non-significant at the 0.05 level

# Summary of the Empirical Assessment of Resistance to IS implementation Model

Path coefficients, explained variance, and statistical significance from three structural models are shown in Table 30. PSE, PP, and PI were hypothesized to be determinants of RTA. It appears that PP statistically significantly determined RTA in all three cases. It could be assumed that an individual with a higher level of power in an organization tends to develop resistance attitude towards the system implementation.

Moreover, the perception of inequity would lead an individual to have a high resistance attitude during the phase of implementation. However, the variance in RTA jointly explained by these three constructs was approximately about 25% – 30%. The degree of explained variance was not very high.

Table 30 Summary of structural model path coefficients and explained variance of the empirical assessment of resistance to change model

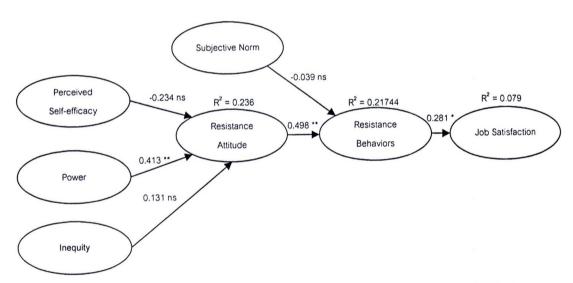
	Structural model path coefficients		
	POSTAL	ENERGY	WATER
PSE → RTA	-0.234 ns	-0.120 ns	-0.212 ns
PP → RTA	0.413 **	0.182 **	0.327 **
PI → RTA	0.131 ns	0.220 **	0.036 ns
SN → RTB	- 0.049 ns	0.075 ns	0.034 ns
RTA → RTB	0.506 **	0.563 **	0.498 **
Variance explained in RTA	23.6%	10.2%	12.9%
Variance explained in RTB	25.1%	31.7%	24.6%

# 4.4.5 Empirical Assessment of Resistance to Change Predicting Job-related Outcomes

One of the research objectives was to examine the consequences of user resistance in the context of mandatory-usage. Resistance behaviors were expected to negatively influence job-related outcomes. This will help to understand how resistance to IS implementation would affect job-related outcomes in this particular context.

#### **POSTAL**

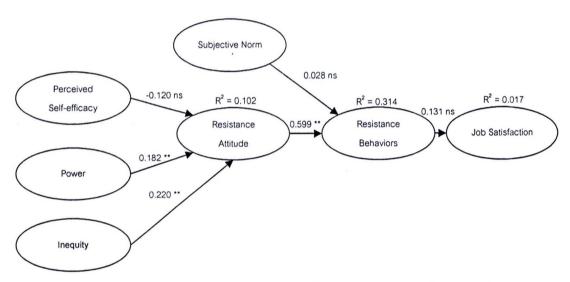
JS was found to be positively directly related to RTB (t = 2.203, p < 0.05). The variance in JS was explained by RTB about 7.9%. SN was not directly related to RTB (t = 0.393, p > 0.05). Only RTA was found to be a primary determinant of RTB (t = 4.709, p < 0.01). Only PP, one of three hypothesized antecedents of RTA, was statistically significantly related to RTA (t = 4.503, p < 0.01).



\* p < 0.01, \*\* p < 0.05, ns : non-significant at the 0.05 level

#### **ENERGY**

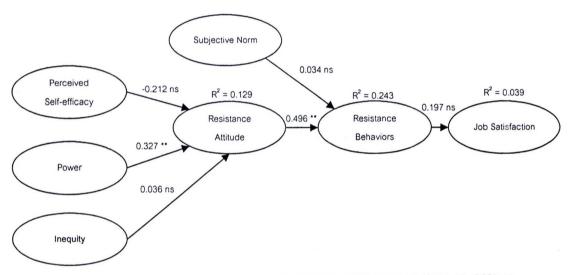
Similar to the results found in the case of POSTAL, RTB was not statistically significantly correlated with JS (t = 1.649, p > 0.05). RTB was statistically significantly determined only by RTA (t = 12.423, p < 0.01) since the relationship between SN and RTB was not significant (t = 0.526, p > 0.05). RTA was directly influenced by PP and PI (t = 2.774, p < 0.01 and t = 3.707, p < 0.01).



\* p < 0.01, \*\* p < 0.05, ns : non-significant at the 0.05 level

#### WATER

The relationship between RTB and JS was not statistically significant (t = 0.900, p > 0.05). About 2.3% of variance in JS was explained by RTB. The relationship between RTA and RTB was moderate (b = 0.496, t = 5.123, p < 0.01). SN was not statistically significantly related to RTB (t = 0.370, p > 0.05). Only PP was significantly correlated with RTA (t = 2.816, p < 0.01). However, PSE and PI, the other hypothesize determinants, did not significantly influence RTA (t = 1.179, p > 0.05 and t = 0.264, p > 0.05).



\* p < 0.01, \*\* p < 0.05, ns : non-significant at the 0.05 level

Summary of the Empirical Assessment of Resistance to Change Predicting Job-related Outcomes

Table 31 provides path coefficients, explained variance, and statistical significance from three structural models. The relationship between JS and RTB were insignificant in the case of ENERGY and WATER. However, when the link was significant in the case of POSTAL, RTB was positively related to JS. The interpretation derived from the results would lead to the idea that an individual who expresses resistance behaviors tends to have higher job satisfaction. This argument could provoke debate and encourage criticism. At this point, it would be inaccurate to presume the positive relationship between resistance to IS implementation and job-related outcomes. Further analysis will be conducted to examine this link.

Table 31 Summary of structural model path coefficients and explained variance of the empirical assessment of resistance to change predicting job-related outcomes

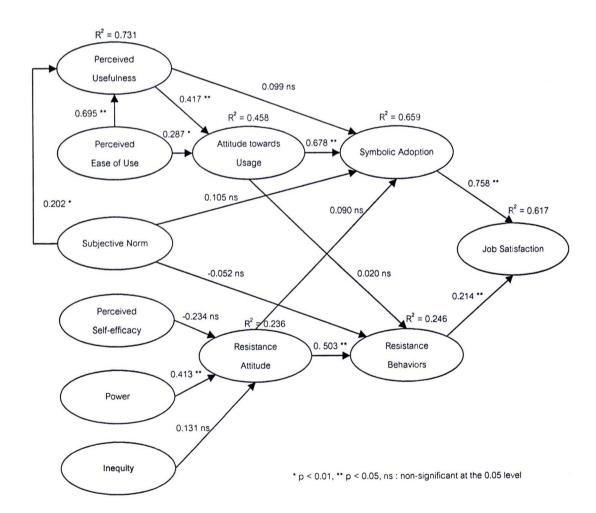
	Structural model path coefficients		
	POSTAL	ENERGY	WATER
PSE → RTA	-0.234 ns	-0.120 ns	-0.212 ns
PP → RTA	0.413 **	0.182 **	0.327 **
PI → RTA	0.131 ns	0.220 **	0.036 ns
SN → RTB	-0.039 ns	0.028 ns	0.034 ns
RTA → RTB	0.498 **	0.559 **	0.496 **
RTB → JS	0.281 *	0.131 ns	0.187 ns
Variance explained in RTA	23.6%	10.2%	12.9%
Variance explained in RTB	24.4%	31.4%	24.3%
Variance explained in JS	7.9%	1.7%	3.9%

#### 4.4.6 Empirical Assessment of the Proposed Model

This section presents the empirical assessment of the model proposed in this study. Three concepts, which are user acceptance, user resistance, and job-related outcomes, are linked together. This is to examine how user acceptance and user resistance are inter-related and jointly affect job-related outcomes. To examine the link between user acceptance and user resistance, the relationships between ATU and RTB, and between RTA and SA are statistically assessed.

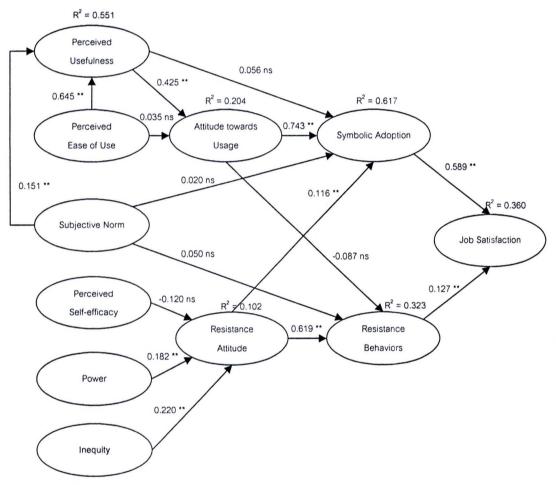
#### **POSTAL**

ATU did not statistically significantly determine RTB (t = 0.174, p > 0.05). Neither did RTA statistically significantly affect SA (t = 1.242, p > 0.05). RTA and ATU explain the variance in SA and RTB, about 65.9% and 24.6%, respectively. SA and RTB were positively statistically significantly related to JS (t = 15.277, p < 0.01 and t = 3.429, p < 0.01).



#### **ENERGY**

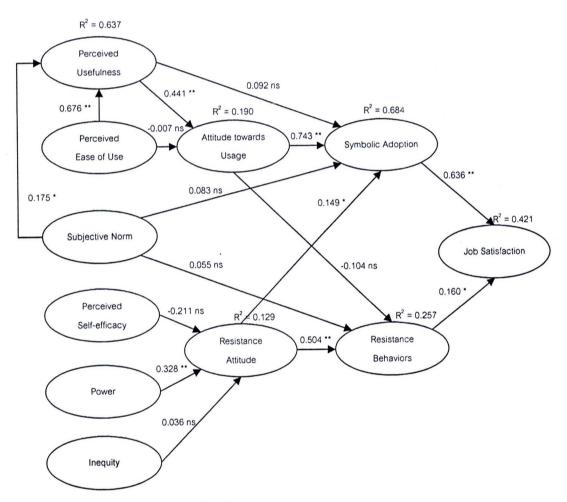
The relationship between ATU and RTB was not statistically significant (t = 1.167, p > 0.05). However, RTA was positively significantly related to SA (t = 2.654, p < 0.01). RTA and ATU explained the variance in SA and RTB, about 61.7% and 32.3%, respectively. Moreover, SA and RTB were positively statistically significantly related to JS (t = 9.172, p < 0.01 and t = 2.603, p < 0.01).



\* p < 0.01, \*\* p < 0.05, ns : non-significant at the 0.05 level

#### **WATER**

RTA was positively significantly related to SA (t = 2.356, p < 0.05), whereas ATU was not significantly related to RTB (t = 0.803, p > 0.05). RTA and ATU mutually explained the variance in SA and RTB, about 68.4% and 25.7%, respectively. SA and RTB were statistically significantly related to JS (t = 7.471, p < 0.01 and t = 2.011, p < 0.01).



\* p < 0.01, \*\* p < 0.05, ns : non-significant at the 0.05 level

#### Summary of the Empirical Assessment of the Proposed Model

Table 32 provides path coefficients, explained variance, and statistical significance from three structural models. Some important findings are significant and should be emphasized: the effects of user acceptance on job-related outcomes, the effects of user resistance on job-related outcomes, and the relationship between user acceptance and user resistance.

First, the effects of user acceptance were found to be positive. SA was positively statistically significantly related to JS in all cases. It appears that a user who agrees with the idea of using the system will be more satisfied with the ERP jobs. The effects of user acceptance, represented by the level of symbolic adoption, tend to have a positive effect on job-related outcomes.

Second, the effects of user resistance were found to be positive. In all cases, RTB was positively statistically significantly correlated to JS. Intuitively, the effects of resistance to IS implementation would be negative. Resistance to IS implementation would lead individuals to be dissatisfied with, or retract from, their jobs on ERP. Hence, individuals with high resistance to IS implementation would lead to low job satisfaction. The findings here show contrasting results. It may be argued that an individual might be satisfied with the job on ERP after they could freely express resistance behaviors such as protesting or complaining. However, there could be the interaction effect between the effects of user acceptance and user resistance on job satisfaction which will be tested in the next section.

Third, the effects of user acceptance on user resistance were not significant in three cases. It appears that positive attitude towards system usage would not help decrease individual resistance behaviors. Even though users agree to the idea of using the system, their acceptance of this particular system will not discourage them to express their resistance behaviors.

Fourth, the effects of user resistance on user acceptance were found inconsistence among three cases. RTA positively significantly influenced SA in the case

of ENERGY and WATER. This may seem to contrast a general belief because resistance attitude is mostly perceived to be negative. It is least likely that negative thoughts and feelings would increase a degree of symbolic adoption. These effects will be explored in the next section.

The effects of user resistance on user acceptance were found to contrast general intuitions. This may stem from the asymmetric effects of resistance (Bhattacherjee and Hikmet, 2007) that makes the relationship between these two concepts perplexing. Further analysis will be performed in the next section to investigate the interaction between user acceptance and user resistance.



Table 32 Summary of structural model path coefficients and explained variance of the proposed model

-	Structural model path coefficients		
	POSTAL	ENERGY	WATER
PEU → PU	0.695 **	0.645 **	0.676 **
SN → PU	0.202 *	0.151 **	0.175 *
PEU → ATU	0.287 *	0.035 ns	-0.042 ns
PU → ATU	0.417 **	0.425 **	0.441 **
PU → SA	0.099 ns	0.054 ns	0.092 ns
ATU → SA	0.678 **	0.743 **	0.743 **
SN → SA	0.105 ns	0.020 ns	0.083 ns
RTA → SA	0.020 ns	0.116 **	0.149 *
PSE → RTA	-0.234 ns	-0.120 ns	-0.211ns
PP → RTA	0.413 **	0.182 **	0.328 **
PI → RTA	0.131 ns	0.220 **	0.036 ns
SN → RTB	-0.052 ns	0.050 ns	0.055 ns
RTA → RTB	0.503 **	0.563 **	0.504 **
ATU → RTB	0.020 ns	-0.087 ns	-0.104 ns
SA → JS	0.758 **	0.589 **	0.636 **
RTB → JS	0.214 **	0.127 **	0.160 *
Variance explained in PU	73.1%	55.1%	63.7%
Variance explained in ATU	45.8%	20.4%	19.0%
Variance explained in SA	65.9%	61.7%	68.4%
Variance explained in RTA	23.6%	10.2%	12.9%
Variance explained in RTB	24.6%	32.3%	25.7%
Variance explained in JS	61.7%	36.0%	42.1%

#### 4.4.7 Empirical Assessment of the Proposed Model with Interaction Effects

From the results found in the empirical assessment of the proposed model shown in the previous section, an issue was posed by the relationship between user acceptance and user resistance. Previous studies have found that the effects of user resistance are asymmetric. Cenfetelli (2004b) posited that inhibitors solely discourage usage. However, the lack of inhibitors would not encourage system adoption. Following this theoretical contention, Bhattacherjee and Hikmet (2007) argue that resistance should not be viewed as non-usage. Especially in this particular context where system usage is mandatory, there should not be non-usage. Hence, the relationship between user acceptance and user resistance should not be viewed as simplistic. The interaction between user acceptance and user resistance could be expected.

The form of the relationships between user acceptance and user resistance should be modeled to include interaction effects. Thus, user acceptance could be moderated by user resistance. Since resistance to IS implementation could be expressed passively or actively, user acceptance might be moderated by either resistance attitude or resistance behaviors. How user acceptance is moderated by user resistance would follow theoretical conceptualization. Symbolic adoption is argued to be determined by user attitude. Hence, it should be mainly influenced by user attitude towards system usage and moderated by resistance attitude. Moreover, the relationship between job-related outcomes and symbolic adoption could be moderated by resistance behaviors. In order to empirically assess the moderating role of resistance to IS implementation, the PLS models with data from the three cases were tested.

In order to test an interaction effect, this study follows fundamental guidelines suggested by Baron and Kenny (1986). The product variable of the independent variable and the moderator is created in order to use in the PLS models. An interaction effect can be obtained by the built-in feature of smartPLS. The analyses for interaction effects in this study also followed the method illustrated in the study

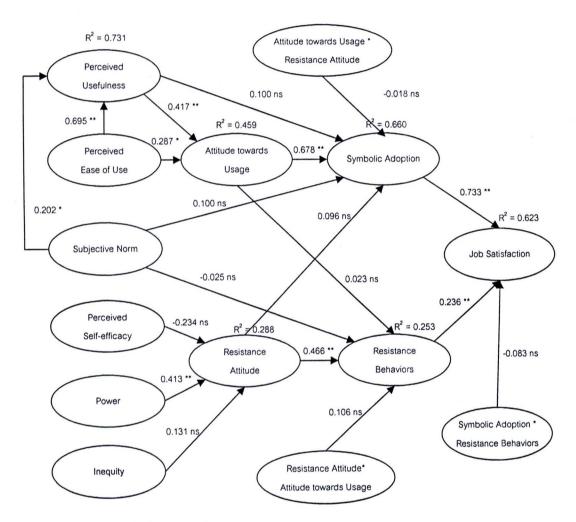
conducted by Chin et al. (1996). Item scores were standardized before multiplication, and then the PLS procedure was used to estimate the interaction effect.

The three moderating effects were introduced into the proposed models: resistance attitude moderating the relationship between attitude towards usage and symbolic adoption, attitude towards usage moderating the relationship between resistance attitude and resistance behaviors, and resistance moderating the relationship between symbolic adoption and job satisfaction. These three interaction effects were created and entered into the proposed model. The PLS models were tested with the three case data separately.

Carte and Russell (2003) indicated nine common errors in testing moderation effects. One group of the errors deals with the inappropriate use and interpretation of statistics. The authors also suggested that the change in R-square should be used as the index of moderator effect size instead of the path coefficients. In addition, the path coefficient of the main effect should not be interpreted when the moderating effect is significant (Carte and Russell, 2003; Venkatesh et al., 2003).

#### **POSTAL**

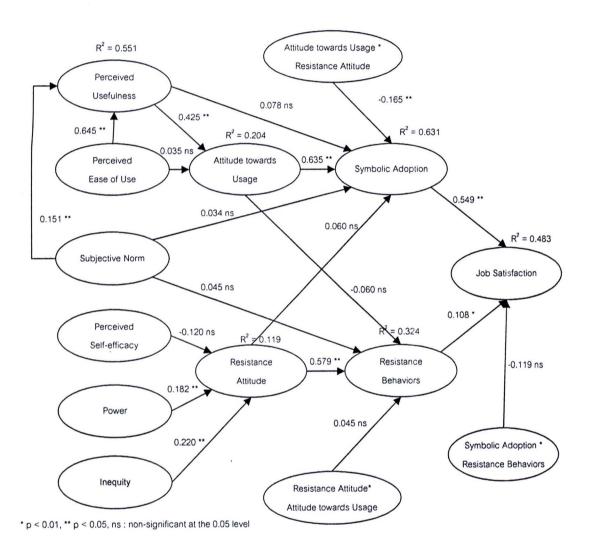
No interaction effects were significant. The interaction effect of ATU and RTA on SA was not significant (t = 0.194, p > 0.05). RTA did not moderate the relationship between ATU and SA (t = 0.583, p > 0.05). The interaction term between SA and RTB was not significantly related to JS (t = 0.800, p > 0.05).



\* p < 0.01, \*\* p < 0.05, ns : non-significant at the 0.05 level

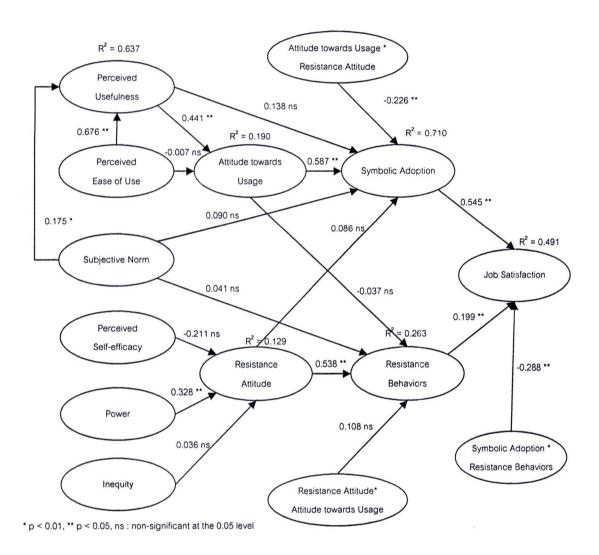
## **ENERGY**

Only one interaction effect was found to be significant. RTA negatively moderated the relationship between ATU and SA (t=2.664, p<0.01). The interaction effect of RTA and ATU on RTB was not significant (t=0.477, p>0.05). RTB did not moderate the relationship between SA and JS (t=1.691, p>0.05).



#### WATER

Only one interaction effect was insignificant. This is the interaction effect of RTA and ATU on RTB (t=0.440, p>0.05). For the significant interaction effects, the interaction effect of ATU and RTA on SA was significant (t=2.665, p<0.01), and the interaction effect between SA and RTB on JS was significant (t=2.189, p<0.05).



# Summary of the Empirical Assessment of the Proposed Model with Interaction Effects

Table 33 presents path coefficients, explained variance, and statistical significance from three structural models testing the interaction effects. The results from the three cases are inconsistent. In the case of POSTAL, no interaction effects were significant. RTA appears to negatively moderate the relationship between ATU and SA in the case of ENERGY and WATER. This means the higher the RTA, the weaker this relationship. Only in the case of WATER, RTB negatively moderated the effects of SA on JS. The R-square change was 7% (from 42.1% to 49.1%). With the interaction effect taken into account, it seems that resistance behaviors could weaken the positive effects of symbolic adoption on job satisfaction.

Table 33 Summary of structural model path coefficients and explained variance of the proposed model with interaction effects

	Structural model path coefficients		
	POSTAL	ENERGY	WATER
PEU → PU	0.695 **	0.645 **	0.676 **
SN → PU	0.202 *	0.151 **	0.175 *
PEU → ATU	0.287 *	0.035 ns	-0.007 ns
PU → ATU	0.417 **	0.425 **	0.441 **
PU → SA	0.100 ns	0.078 ns	0.138 ns
ATU → SA	0.678 **	0.635 **	0.587 **
SN → SA	0.100 ns	0.034 ns	0.090 ns
RTA → SA	0.020 ns	0.060 ns	0.086 ns
ATU*RTA → SA	-0.018 ns	-0.165 **	-0.226 *
PSE → RTA	-0.234 ns	-0.120 ns	-0.211 ns
PP → RTA	0.413 **	0.182 **	0.328 **
PI → RTA	0.131 ns	0.220 **	0.036 ns
SN → RTB	-0.025 ns	0.045 ns	0.041 ns
RTA → RTB	0.466 **	0.579 **	0.538 **
ATU → RTB	0.023 ns	-0.060 ns	-0.037 ns
RTA*ATU → RTB	0.106 ns	0.045 ns	0.108 ns
SA → JS	0.733 **	0.549 **	0.545 **
RTB → JS	0.236 **	0.108 *	0.199 *
SA*RTB → JS	-0.083 ns	-0.119 ns	-0.288 **
Variance explained in PU	73.1%	55.1%	63.7%
Variance explained in ATU	45.9%	20.4%	19.0%
Variance explained in SA	66.0%	63.1%	71.0%
Variance explained in RTA	23.6%	10.2%	12.9%
Variance explained in RTB	25.3%	32.4%	26.3%
Variance explained in JS	62.3%	37.2%	49.1%

# 4.5 Summary of Chapter IV

A PLS approach to SEM was employed to empirically assess the proposed theoretical framework. The results of data analysis were presented. The next chapter will discuss the results and conclude the findings of the present study.