CHAPTER IV RESULTS AND DISCUSSION

4.1 Mixed Matrix Membranes of Silicone Rubber and Activated Carbon

The permeabilities of carbon dioxide, P_{CO_2}/d ; nitrogen, P_{N_2}/d ; hydrogen, P_{H_1}/d ; propane, $P_{C_3H_8}/d$; propylene, $P_{C_3H_6}/d$ and the selectivity of carbon dioxide to nitrogen, P_{CO2}/P_{N2} ; carbon dioxide to hydrogen, P_{CO2}/P_{H2} ; and propylene to propane, P_{C3H6}/P_{C3H8} were determined from steady state permeation rates of each gas through the membrane at room temperature and pressures between 5 and 100 psia to investigate the selectivities and plasticization phenomenon.

4.1.1 <u>Selectivities of Gases through Silicone Rubber Membrane and</u> <u>Activated Carbon/Silicone Rubber MMM</u>

Table 4.1 Selectivities of gases through membrane prepared from silicone rubber/polysulfone and various loading activated carbon/silicone rubber/polysulfone MMM (measured the fluxes at 50 psia)

| Membrane | Selectivity | | | | | |
|---------------------------------------|---------------------------------|---------------------------------|-----------------|--|--|--|
| | CO ₂ /N ₂ | CO ₂ /H ₂ | C_3H_6/C_3H_8 | | | |
| SIL/PS ¹ | 12.069 | 4.574 | 0.876 | | | |
| 10 wt% Act.C./SIL/PS MMM ² | 12.627 | 4.854 | 1.013 | | | |
| 20 wt% Act.C./SIL/PS MMM ² | 15.101 | 4.545 | 1.022 | | | |
| 30 wt% Act.C./SIL/PS MMM ² | 19.167 | 5.982 | 1.057 | | | |

<u>Notes</u>

¹SIL/PS

Silicone rubber coated on porouspolysulfone

X wt% Activated carbon/silicone rubber
coated on porous polysulfone

²X wt% Act.C./SIL/PS MMM

where X = 10, 20, or 30

Silicone rubber/polysulfone membrane and activated carbon/silicone rubber/polysulfone MMM varied amount of activated carbon in 10, 20, and 30 wt% were used to study the selectivity of CO_2/N_2 , CO_2/H_2 , and C_3H_6/C_3H_8 . Testing conditions were room temperature, P = 50 psia and pure gas measurement.

For CO_2/N_2 separation, the result showed that CO_2/N_2 selectivity increased with increasing amount of activated carbon. From adsorption isotherms of CO_2 and N_2 on activated carbon at 300 K as shown in Figure 4.1, CO_2 can adsorb on activated carbon more than N_2 over 100-1500 Torr. Therefore, increasing amount of activated carbon in silicone rubber/polysulfone membrane will allow CO_2 to be adsorbed and pass through the membrane faster than N_2 .



Figure 4.1 Adsorption isotherms of CO₂ and N₂ on activated carbon at 300 K (Low Temperature Measurements Group, 1962 (TM D-11)).

For CO_2/H_2 separation, CO_2/H_2 selectivity increased slightly with increasing amount of activated carbon. From adsorption isotherms of CO_2 and H_2 on activated carbon at 195 K as shown in Figure 4.2(a),(b)at low pressure around 10 Torr activated carbon can adsorb CO_2 around 14g/100g activated carbon which was higher than H_2 that used high pressure around 15000 Torr to adsorb. Therefore, activated carbon can adsorb CO_2 more than H_2 at the same pressure. When increasing amount of activated carbon in silicone rubber membrane, it will increase CO_2 to adsorb and pass through membrane to permeate side faster than H_2 . However the CO_2/H_2 selectivity did not increase significantly, hydrogen molecule was very small. The effect of small hydrogen molecules can help them to pass through the membrane.



Figure 4.2 (a) Adsorption isotherm of CO₂ on activated carbon at 195 K (Temperature Measurements Group, 1962 (TM D-11)).



Figure 4.2 (b) Adsorption isotherm of H_2 on activated carbon at 195 K (Low Temperature Measurements Group, 1962 (TM D-11)).

For C_3H_6/C_3H_8 separation, silicone rubber/polysulfone membrane was selective for propane, but adding activated carbon in silicone rubber/polysulfone membrane can change the selectivity from propane to propylene. Silicone rubber/polysulfone membrane was selective for propylene after adding 10, 20 and 30 wt% activated carbon. From adsorption isotherms of C_3H_6 and C_3H_8 on activated carbon at 298 K as shown in Figure 4.3, propylene can adsorb on activated carbon more than propane over 100-800 Torr. Therefore, increasing amount of activated carbon in silicone rubber membrane will increase propylene to adsorb and pass through the membrane faster than propane.



Figure 4.3 Adsorption isotherms of C_3H_6 and C_3H_8 on activated carbon at 298 K (Low Temperature Measurements Group, 1962 (TM D-11)).

4.1.2 Effects of pressure to membrane permeabilities

It was found from the literature that polymeric membrane can occur plasticization (Bos *et al.*, 1999). Plasticization was the one of stability problems in membrane. When plasticization occurred, permeability increased and then membrane lose selectivity. Therefore, in this part silicone rubber/polysulfone membrane and activated carbon/silicone rubber/polysulfone MMM were used to study the effect of pressure to membrane permeabilities by using CO_2 , N_2 , H_2 , C_3H_6 , C_3H_8 as the feed and varying pressures from 5-100 psia.



1) Silicone rubber/polysulfone membrane (SIL/PS)

Figure 4.4 Relation between pressure and permeability of silicone rubber/ polysulfone membrane.

Figure 4.4 shows effect of pressure on silicone rubber/polysulfone membrane permeability. Permeabilities of propylene, propane and carbon dioxide increased with increasing pressure; however, permeabilities of H_2 and N_2 were

relatively constant. The membrane changed C_3H_6/C_3H_8 selectivity from propylene at low pressures to propane at high pressures. Because propylene has smaller effective diameter than propane. The C=C bond which is made up of a strong σ bond and a weak π bond has greater total bond energy (e.g., 146 kcal for ethylene) than the C-C bond (e.g., 88 kcal for ethane). The atoms would be held tighter together where the double bond length is 1.34 A as compared to the single bond length, 1.53 A . Therefore, olefins have higher diffusivity than paraffins of the same C number likely due to the smaller effective diameters for diffusion (Chan *et al.*, 2002). So, at low pressures propylene would be able to diffuse through a membrane faster than propane. However at high pressures the phenomenon is in contrast, in which the membrane is selective to propane. Because the effect of solubility dominated the size effect. The critical temperature of propane is higher than propylene. It meant that propane was more soluble than propylene (Chan *et al.*, 2002). Therefore, propane will pass through membrane faster than propylene at high pressures.

10 wt% Activated carbon/silicone rubber/polysulfone MMM (10 wt%Act.C./SIL/PS MMM)

Figure 4.5 shows effect of pressure on 10 wt%Act.C./SIL/PS MMM permeability. The permeability of propane, propylene and carbon dioxide increased with increasing pressure; however, permeabilities of H_2 and N_2 were relatively constant.



Figure 4.5 Relation between pressure and permeability of 10 wt%Activated carbon/silicone rubber/polysulfone MMM.

In comparison of SIL/PS membrane and 10 wt%Act.C./SIL/PS MMM, the later did not occur the reversibility of C_3H_6/C_3H_8 selectivity. Because activated carbon was selective for propylene more than propane.

Propylene, propane and carbon dioxide were more soluble gases than hydrogen and nitrogen (Chan *et al.*, 2002). Therefore, C_3H_6 , C_3H_8 and CO_2 will be able to plasticize in membrane.

20 wt% Activated carbon/silicone rubber/polysulfone MMM (20 wt% Act.C./SIL/PS MMM)

The result of 20 wt% activated carbon/silicone rubber/polysulfone MMM showed the same trend as 10 wt% activated carbon/silicone rubber/polysulfone MMM.



Figure 4.6 Relation between pressure and permeability of 20 wt%Activated carbon/silicone rubber/polysulfone MMM.

However, adding activated carbon to 30 wt% showed the strong different behavior.

4) 30 wt% Activated carbon/silicone rubber/polysulfone MMM (30 wt% Act.C./SIL/PS MMM)

Figure 4.7 shows the effect of pressure to 30 wt% activated carbon/silicone rubber/polysulfone MMM permeability. At low pressure, permeability of C_3H_6 , C_3H_8 , CO_2 and N_2 sharply decreased with increasing pressure because of hydrostatic compression effect. 30 wt% activated carbon was enough to increase the glassy state in membrane. Therefore, increasing pressure will reduce free volume in membrane and then decrease permeability.



Figure 4.7 Relation between pressure and permeability of 30 wt%Activated carbon/silicone rubber/polysulfone MMM.

However, at high pressure permeability of C_3H_6 and C_3H_8 increased with increasing pressure. CO₂ permeability slowly decreased and H₂, N₂ permeability remained constant. Because propylene and propane were more soluble in membrane than CO₂. So the enough pressure can overcome the compression effect.

About H_2 , N_2 they were the less soluble gases, so pressure did not have the effect to their permeabilities.

4.2 Mixed Matrix Membranes of Silicone Rubber, Activated Carbon and Polyethylene glycol (PEG)

According to the previous work (Charoenphol, 2002), the CO_2/N_2 selectivity increased as the concentration of PEG in the membranes increased and form the first part of my work CO_2/N_2 , CO_2/H_2 and C_3H_6/C_3H_8 selectivities increased with increasing amount of Act.C. Therefore, in order to enhance these selectivities the combined membrane will be created. 20 wt%Act.C./SIL/PS MMM added with PEG from 5, 10 to 15 wt% was investigated for CO_2/N_2 , CO_2/H_2 , and C_3H_6/C_3H_8 separations and have also studied plasticization phenomenon.

4.2.1 <u>Selectivities of Gases through Silicone Rubber/Polysulfone, Activated</u> <u>Carbon/Silicone Rubber/Polysulfone MMM and PEG+Activated</u> <u>Carbon/Silicone Rubber/Polysulfone MMM</u>

Table 4.2 Selectivities of gases through membrane prepared from silicone rubber/polysulfone and various loading of PEG + 20wt%activated carbon/silicone rubber/polysulfone MMM (measured the fluxes at 50psia)

| Membrane | Selectivity | | | |
|---------------------------------|---------------------------------|---------------------------------|--|--|
| | CO ₂ /N ₂ | CO ₂ /H ₂ | C ₃ H ₆ /C ₃ H ₈ | |
| SIL/PS | 12.069 | 4.574 | 0.876 | |
| 20wt%Act.C./SIL/PS MMM | 15.101 | 4.545 | 1.022 | |
| 5wt%PEG+20wt%Act.C./SIL/PS MMM | 10.747 | 4.511 | 0.414 | |
| 10wt%PEG+20wt%Act.C./SIL/PS MMM | 15.420 | 3.250 | 0.382 | |
| 15wt%PEG+20wt%Act.C./SIL/PS MMM | 21.679 | 2.087 | 1.598 | |

Notes

X wt% PEG+20wt%Act.C./SIL/PS MMM = Xwt% PEG + 20wt%Activated carbon/silicone rubber coated on porous polysulfone



where x = 0,5,10 or 15

Amount of PEG added (wt%)

Figure 4.8 Relation between wt% PEG in 20 wt%Activated carbon/silicone rubber/polysulfone MMM and selectivities.

From Table 4.1 the CO₂/N₂, CO₂/H₂ and C₃H₆/C₃H₈ selectivities increased with increasing amount of activated carbon in activated carbon/silicone rubber/polysulfone MMM. In this study, 20wt%activated carbon/silicone rubber/polysulfone MMM was chosen and then adding PEG at 5, 10, 15 wt%. Because this amount of Act.C. can mix with PEG and did not precipitate. So it was suitable for casting the membrane. Besides, to study these three selectivities plasticization phenomenon has been considered. The selectivities are shown in Table 4.2 and Figure 4.8. This experiment was done at room temperature, different pressure = 50 psia and pure gas measurement. The CO_2/N_2 selectivity decreased when adding 5 wt% PEG and then increased when adding 10, 15 wt% PEG in 20wt%activated carbon/silicone rubber/polysulfone MMM. Because little amount of PEG at 5 wt% will adsorb in pore of activated carbon. So PEG will not show the effect to enhance selectivity. From the previous work (Charoenphol, 2002) PEG suspended in silicone rubber/polysulfone membrane improved the CO_2/N_2 selectivity when compared to pure silicone rubber/polysulfone membrane. It can be concluded that the CO_2/N_2 selectivity can be enhanced when PEG suspended in the polymer phase. The other possible reason is change of activated carbon property after adsorbed PEG. The property of activated carbon maybe change after PEG adsorb in activated carbon. So PEG reduced the impact of activated carbon for CO_2/N_2 selectivity.

After adding 10, 15wt% PEG in 20wt%activated carbon/silicone rubber/polysulfone MMM, CO_2/N_2 selectivity increased. Because 10, 15 wt%PEG is enough to adsorb in pore of activated carbon and the rest can suspend in polymer phase to enhance this selectivity.

 CO_2/H_2 selectivity decreased with increasing amount of PEG. Adding PEG in activated carbon/silicone rubber/polysulfone reduced the permeability of gas. Due to the dominance of PEG crystallinity in membrane, it reduced the segmental motion in membrane (Li et al.,). Gas molecule moves harder than without PEG. When compared the reducing in permeability of CO_2 and H_2 , the CO_2 permeability decreased more than the H_2 permeability. Because of smaller molecule of H_2 , it will be able to pass through PEG crystallinity more easily than larger molecule like CO_2 . Therefore CO_2/H_2 selectivity decreased when increasing amount of PEG in PEG /Act.C./SIL/PS MMM, selectivity is the product of permeability shown in Eq. (2.5).

 C_3H_6/C_3H_8 selectivity was lower than one at 5, 10 wt%PEG in PEG /20wt%Act.C./SIL/PS MMM and then increased higher than one and higher than pure 20wt%Act.C./SIL/PS MMM when adding 15 wt%PEG in 20wt%Act.C./SIL/PS MMM. From the last result 20wt%Act.C./SIL/PS MMM was selective for olefin. From the previous work (Sukapintha, 2000) PEG/silicone rubber/polysulfone MMM was selective for olefin. C_2H_4/C_2H_6 selectivity was around 1.70. So mixing PEG and activated carbon in silicone rubber/polysulfone membrane will be possible to enhance olefin/paraffin selectivity. However, the result showed inverse selectivity at

5, 10 wt%PEG and C_3H_6/C_3H_8 selectivity enhanced at 15 wt%PEG. Because little amount of PEG will be able to adsorb in pore of activated carbon. It may change property of activated carbon after PEG adsorb in activated carbon. PEG can enhance C_3H_6/C_3H_8 selectivity when amount of PEG is much enough to have the rest in polymer phase like 15wt%PEG.

Table 4.3 Permeabilities of gases through membrane prepared from siliconerubber/polysulfone membrane and various loading of PEG + 20wt%activatedcarbon/silicone rubber/polysulfone MMM at 50 psia

| Membrane | Permeability (cm ³ /(cm ² .sec.cmHg)) | | | | |
|------------------------------------|---|----------------|----------------|-------------------------------|-------------------------------|
| | CO ₂ | N ₂ | H ₂ | C ₃ H ₆ | C ₃ H ₈ |
| 20wt%Act.C./SIL/PS MMM | 5.158E-5 | 3.416E-6 | 1.135E-5 | 1.518E-4 | 1.486E-4 |
| 5wt%PEG + 20wt%Act.C./SSIL/PS MMM | 1.819E-5 | 1.692E-6 | 0.403E-5 | 0.107E-4 | 0.258E-4 |
| 10wt%PEG + 20wt%Act.C./SSIL/PS MMM | 1.388E-5 | 0.900E-6 | 0.392E-5 | 0.040E-4 | 0.105E-4 |
| 15wt%PEG + 20wt%Act.C./SSIL/PS MMM | 0.695E-5 | 0.320E-6 | 0.333E-5 | 0.003E-4 | 0.002E-4 |

From Table 4.3 the permeabilities of the gases reduced with adding of PEG in 20wt%activated carbon/silicone rubber/polysulfone MMM. One may infer that higher amount of PEG caused denser intersegmental chain packing in MMM. So it is difficult for gas molecule to diffuse in membrane. From the results amount of PEG affected to the decreasing in permeability of C_3H_6 , C_3H_8 more than other gases. Because molecule of C_3H_6 and C_3H_8 are bigger than N₂, CO₂ and H₂. So the larger molecules are, the harder they diffuse.

4.2.2 Effects of Pressure to Membrane Permeabilities

In this part PEG / 20wt%Act.C./SIL/PS MMM was used to investigate the effect of amount of PEG on plasticization by using CO₂, N₂, H₂, C₃H₆ and C₃H₈ as the feed and varying pressures from 5 – 100 psia.



Figure 4.9 Relation between pressure and C₃H₈ permeability in 5, 10, 15 wt%PEG/20 wt%Act.C./SIL/PS MMM.

2) C_3H_6 permeability



Figure 4.10 Relation between pressure and C₃H₆ permeability in 5, 10, 15 wt%PEG/20 wt%Act.C./SIL/PS MMM.

3) CO₂ permeability



Figure 4.11 Relation between pressure and CO₂ permeability in 5, 10, 15 wt%PEG/20 wt%Act.C./SIL/PS MMM.

Figures 4.9-4.11 shows effect of amount of PEG on C_3H_8 , C_3H_6 and CO_2 plasticization, respectively. The plasticization of three gases shows the same trend because they are more soluble. The plasticization of them decreased with increasing the amount of PEG. This is because adding PEG will reduce free volume in the membrane resulting in difficulty for gas molecules to solute and plasticize in membrane.

4) N₂ permeability

Figure 4.12 shows effect of amount of PEG on N_2 plasticization. The plasticization of N_2 shows the different trade with C_3H_8 , C_3H_6 and CO_2 . N_2 permeability decreased with increasing pressure when adding PEG at 5 and 10 wt% because of hydrostatic compression effect. For less soluble gas like N2, H2 they are hard to plasticize in membrane and adding PEG will increase crystallinity in membrane. It means that PEG reduces the flexibility of polymer chains. Therefore, when increasing pressure, it reduces the free volume in membrane and then decreasing permeability.

However, adding PEG to 15 wt% shows the plasticization of N2 in membrane. One may infer that the large amount of PEG will be able to increase the rubbery state in membrane. Because PEG itself may be more flexible than polymer chain.



Figure 4.12 Relation between pressure and N₂ permeability in 5, 10, 15 wt%PEG/20 wt%Act.C./SIL/PS MMM.

5) H₂ permeability

Figure 4.13 shows effect of amount of PEG on H_2 plasticization. Although H_2 is less soluble gas like N_2 , it can plasticize in membrane. Because H_2 molecule is smaller than N2. It can use this benefit to plasticize in membrane.



Figure 4.13 Relation between pressure and H₂ permeability in 5, 10, 15 wt%PEG/20 wt%Act.C./SIL/PS MMM.