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APPENDICES

Calculation of cobalt loading

Preparation of 20%wtCo/SiO₂ by the incipient wetness impregnation method was shown as follow:

Reagent: - Cobalt (II) nitrate hexahydrate (Co(NO₃)₂·6H₂O)
 Molecular weight = 291.03 g/mol
 Cobalt (Co), Atomic weight = 58.933 g/mol
 - Support: - spherical silica support

Based on 1.00 g of catalyst used, the composition of the catalyst would be as follows:

$$\begin{aligned} \text{Cobalt} &= 0.20 \text{ g} \\ \text{SiO}_2 &= 1.00 - 0.20 = 0.80 \text{ g} \end{aligned}$$

Cobalt 0.20 g was prepared from Cobalt (II) nitrate hexahydrate

$$\begin{aligned} \text{Cobalt (II) nitrate hexahydrate required} &= \frac{0.20}{58.933} \times 291.03 \\ &= 0.9877 \text{ g} \end{aligned}$$

APPENDIX B

CALCULATION FOR TOTAL CO CHEMISORPTION AND DISPERSION

Calculation of the total CO chemisorption and metal dispersion of the catalyst, a stoichiometry of CO/Co = 1, was assumed. The calculation procedure was as follows:

Let the weight of catalyst used	=	W	g
Integral area of CO peak after adsorption	=	A	unit
Integral area of 100 μ l of standard H ₂ peak	=	B	unit
Amounts of CO adsorbed on catalyst	=	B-A	unit
Concentration of Co	=	C	%wt
Volume of H ₂ adsorbed on catalyst	=	100 \times [(B-A)/B]	μ l
Volume of 1 mole of CO at 30 $^{\circ}$ C	=	24.86 $\times 10^6$	μ l
Mole of CO adsorbed on catalyst	=	[(B-A)/B] \times [100/24.86]	μ mole
Total CO chemisorption	=		
		[(B-A)/B] \times [100/29.93] \times [1/W]	μ mole /g _{catalyst}
	=	N	μ mole /g _{catalyst}

$$\%Co \text{ dispersion} = \frac{\text{The amount of cobalt equivalent to CO adsorption after reduction} \times 100}{\text{Total amount of cobalt active sites expected to exist after reduction}}$$

Molecular weight of cobalt	=	58.93
Metal dispersion (%)	=	$\frac{1 \times CO_{tot} \times 100}{No. \mu mole Co_{tot}}$
	=	$\frac{1 \times N \times 100}{No. \mu mole Co_{tot}}$
	=	$\frac{1 \times N \times 58.93 \times 100 \times 100}{[C \times 10^6]}$
	=	$\frac{0.59 \times N}{C}$

APPENDIX C

CALCULATION FOR REDUCIBILITY

For supported cobalt catalyst, it can be assumed that the major species of calcined Co catalysts was Co_3O_4 . H_2 consumption to reduce Co_3O_4 was calculated as follows:

$$\text{Molecular weight of Co} = 58.93$$

$$\text{Molecular weight of } \text{Co}_3\text{O}_4 = 240.79$$

Calculation of the calibration of H_2 consumption using cobalt oxide (Co_3O_4)

$$\begin{aligned} \text{Let the weight of } \text{Co}_3\text{O}_4 \text{ used} &= 0.1 \text{ g} \\ &= 4.153 \times 10^{-4} \text{ mole} \end{aligned}$$

From equation of Co_3O_4 reduction;



$$\begin{aligned} \text{Mole of hydrogen consumption} &= 4 \text{ Mole of } \text{Co}_3\text{O}_4 \text{ consumption} \\ &= 4 \times 4.153 \times 10^{-4} \\ &= 1.661 \times 10^{-3} \text{ mole} \end{aligned}$$

Integral area of hydrogen used to reduce Co_3O_4 0.1 g = 115.63 unit

At 100 % reducibility, the amount of hydrogen consumption is 1.661×10^{-3} mole related to the integral area of Co_3O_4 after reduction 115.63 unit.

Calculation of reducibility of supported cobalt catalyst

$$\% \text{ Reducibility} = \frac{\text{Amount of } \text{H}_2 \text{ uptake to reduce 1 g of catalyst} \times 100}{\text{Amount of theoretical } \text{H}_2 \text{ uptake to reduce } \text{Co}_3\text{O}_4 \text{ to } \text{Co}^0 \text{ for 1 g of catalyst}}$$

Integral area of the calcined catalyst	=	X	unit
The amount of H ₂ consumption	=		
$\left[2 \times 1.661 \times 10^{-3} \times (X) / 115.63\right]$ mole			
Let the weight of calcined catalyst used	=	W	g
Concentration of Co	=	Y	%wt
Mole of Co	=	$[(W \times Y / 100) / 58.93]$	mole
Mole of Co ₃ O ₄	=	$[(W \times Y / 100) / (3 \times 58.93)]$	mole
Amount of theoretical	=	$[(W \times Y / 100) \times 4 / (3 \times 58.93)]$	mole
Reducibility (%) of supported Co catalyst	=		
$\frac{\left[2 \times 1.661 \times 10^{-3} \times (X) / 115.63\right] \times 100}{[(W \times Y / 100) \times 4 / (3 \times 58.93)]}$			



Example for 20Co/ Z

<i>Integral area of the calcined catalyst</i>	=	6.016	unit
<i>The amount of H₂ consumption</i>	=	$\left[2 \times 1.661 \times 10^{-3} \times (X) / 115.63\right]$	mole
<i>Let the weight of calcined catalyst used</i>	=	0.1	g
<i>Concentration of Co</i>	=	20	%wt
<i>Mole of Co</i>	=	$[(0.1 \times 20 / 100) / 58.93]$	mole
<i>Mole of Co₃O₄</i>	=	$[(0.1 \times 20 / 100) / (3 \times 58.93)]$	mole
<i>Amount of theoretical</i>	=	$[(0.1 \times 20 / 100) \times 4 / (3 \times 58.93)]$	mole
<i>Reducibility (%) of supported Co catalyst</i>	=		
$\frac{\left[2 \times 1.661 \times 10^{-3} \times (6.016) / 115.63\right] \times 100}{[(0.1 \times 20 / 100) \times 4 / (3 \times 58.93)]}$	=	34.6	%

APPENDIX D

CALIBRATION CURVES

This appendix showed the calibration curves for calculation of composition of reactant and products in CO hydrogenation reaction. The reactant is CO and the main product is methane. The other products are linear hydrocarbons of heavier molecular weight that are C₂-C₄ such as ethane, ethylene, propane, propylene and butane.

The thermal conductivity detector, gas chromatography Shimadzu model 8A was used to analyze the concentration of CO by using Molecular sieve 5A column.

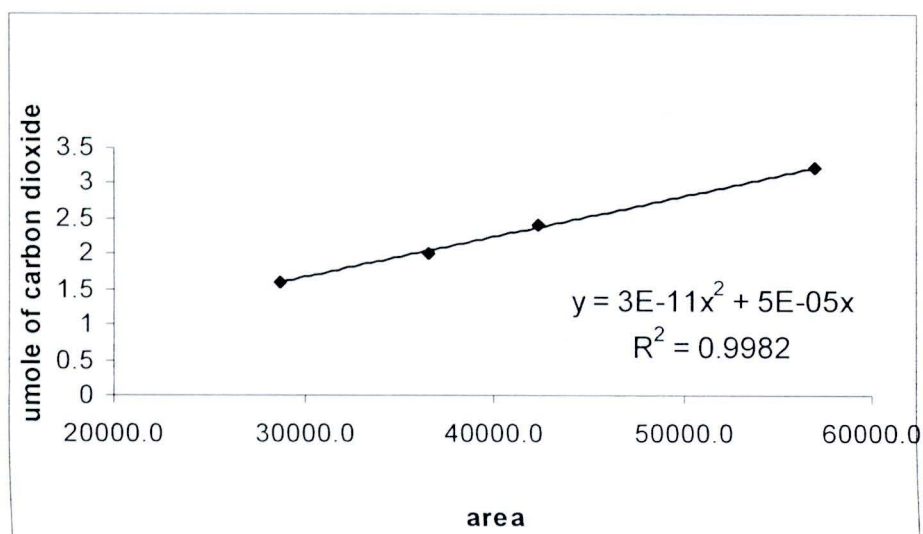
The thermal conductivity detector (TCD), gas chromatography Shimadzu model 8A was used to analyze the concentration of CO₂ by using porapack-Q column.

The VZ10 column are used with a gas chromatography equipped with a flame ionization detector, Shimadzu model 14B, to analyze the concentration of products including of methane, ethane, ethylene, propane, propylene and butane. Conditions uses in both GC are illustrated in Table C.1.

Mole of reagent in y-axis and area reported by gas chromatography in x-axis are exhibited in the curves. The calibration curves of CO, methane, ethane, ethylene, propane, propylene and butane are illustrated in the following figures.

Table D.1 Conditions use in Shimadzu modal GC-8A and GC-14B.

Parameters	Condition	
	Shimadzu GC-8A	Shimadzu GC-14B
Width	5	5
Slope	50	50
Drift	0	0
Min. area	10	10
T.DBL	0	0
Stop time	50	60
Atten	0	0
Speed	2	2
Method	41	41
Format	1	1
SPL.WT	100	100
IS.WT	1	1

**Figure D.1** The calibration curve of carbon dioxide.

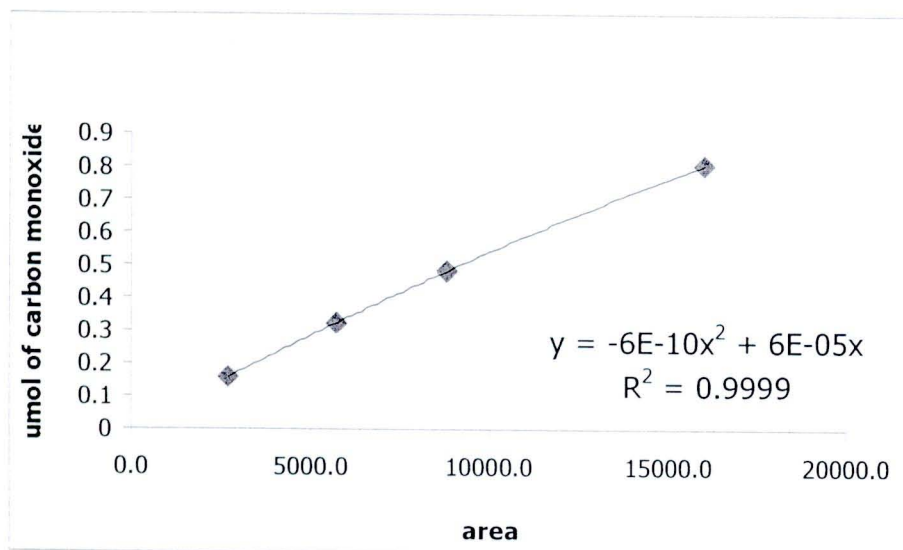


Figure D.2 The calibration curve of carbon monoxide.

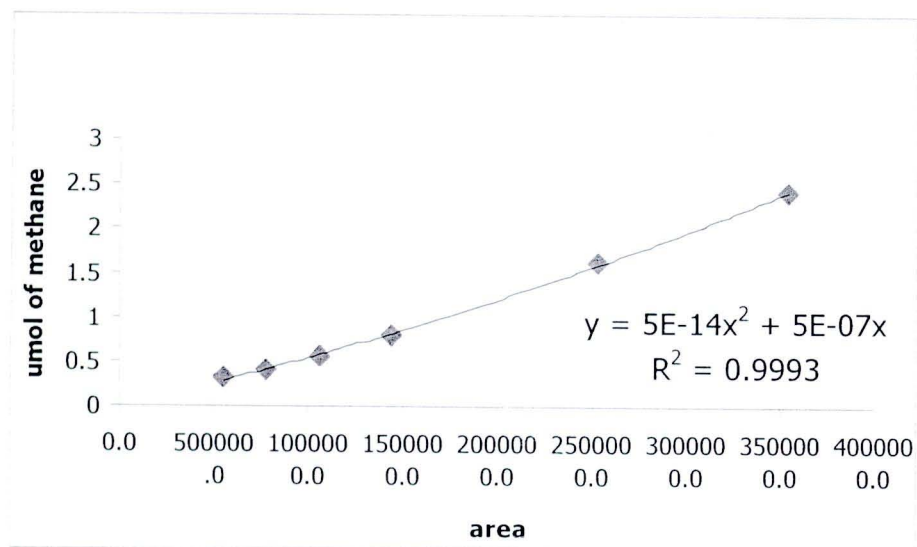


Figure D.3 The calibration curve of methane.

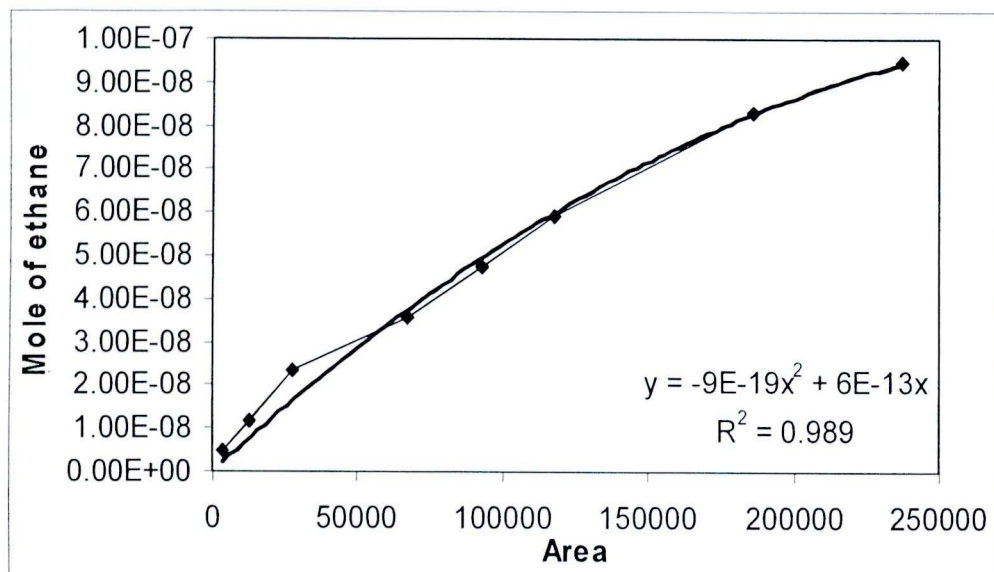


Figure D.4 The calibration curve of ethane.

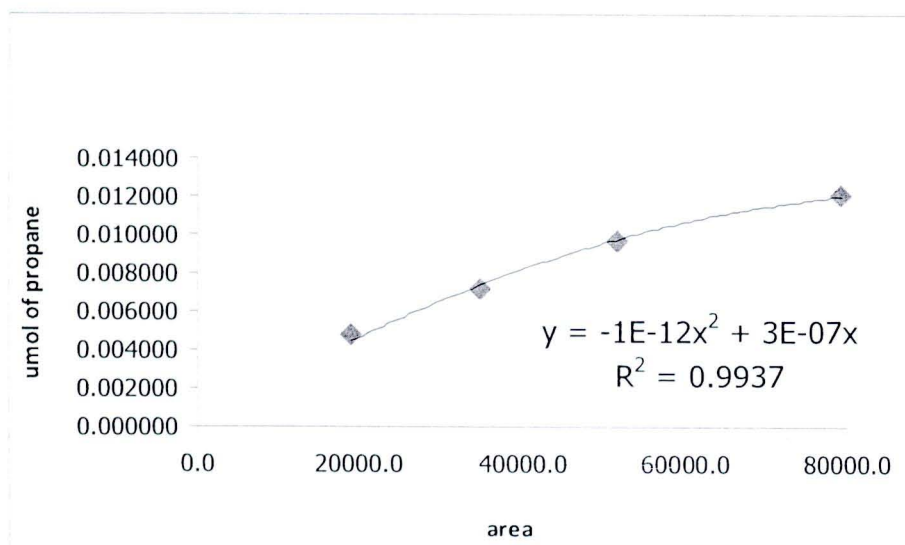


Figure D.5 The calibration curve of propane.

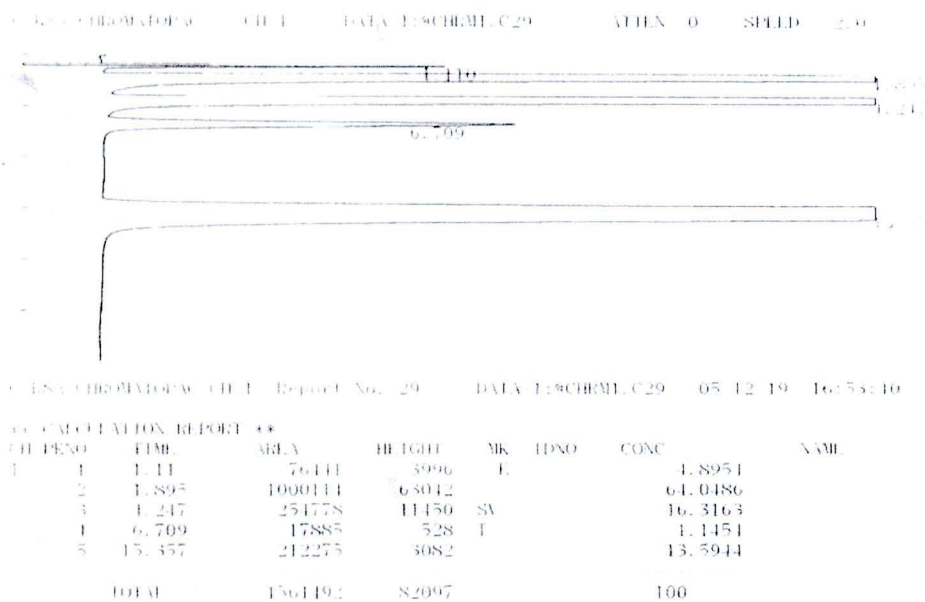


Figure D.6 The chromatograms of catalyst sample from thermal conductivity detector, gas chromatography Shimadzu model 8A (Molecular sieve 5A column).

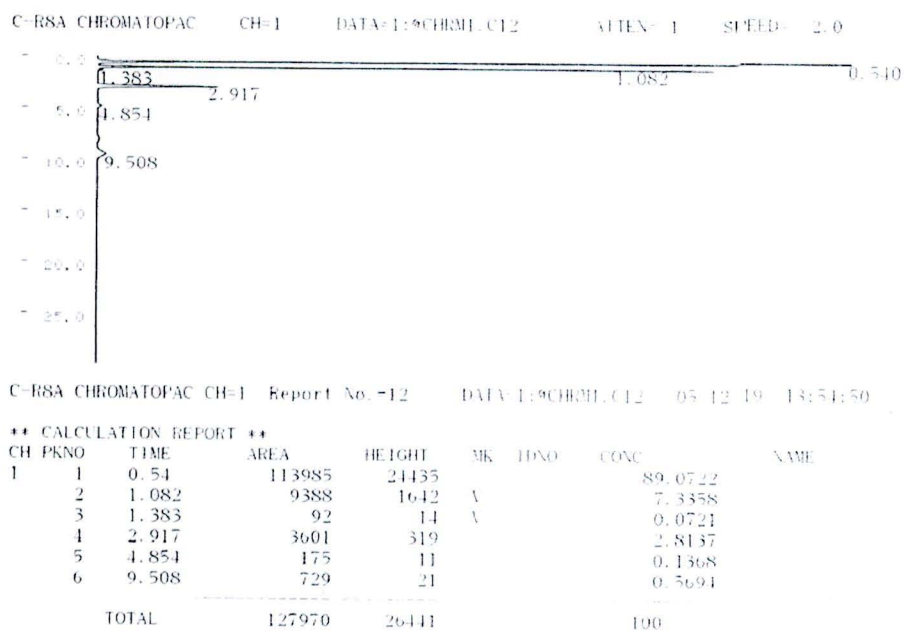


Figure D.7 The chromatograms of catalyst sample from flame ionization detector, gas chromatography Shimadzu model 14B (VZ10 column).

APPENDIX E

CALCULATION OF CO₂ CONVERSION, REACTION RATE AND SELECTIVITY

The catalyst performance for the CO₂ hydrogenation was evaluated in term of activity for CO₂ conversion, reaction rate and selectivity.

CO₂ conversion is defined as moles of CO₂ converted with respect to CO₂ in feed:

$$\text{CO}_2 \text{ conversion (\%)} = \frac{100 \times [\text{mole of CO}_2 \text{ in feed} - \text{mole of CO}_2 \text{ in product}]}{\text{mole of CO}_2 \text{ in feed}} \quad (\text{i})$$

Reaction rate was calculated from CO₂ conversion that is as follows:

Let the weight of catalyst used	=	W	g
Flow rate of CO ₂	=	2	cc/min
Reaction time	=	60	min
Weight of CH ₂	=	14	g
Volume of 1 mole of gas at 1 atm	=	22400	cc
Selectivity to CH ₄	=	S	

$$\text{Reaction rate (g CH}_2\text{/g of catalyst.h)} = \frac{(\% \text{ conversion of CO}_2 / 100) \times 60 \times 14 \times 2}{W \times 22400} \times S \quad (\text{ii})$$

Selectivity of product is defined as mole of product (B) formed with respect to mole of CO₂ converted:

$$\text{Selectivity of B (\%)} = 100 \times [\text{mole of B formed} / \text{mole of total products}] \quad (\text{iii})$$

Where B is product, mole of B can be measured employing the calibration curve of products such as methane, ethane, ethylene, propane, propylene and butane

$$\text{mole of CH}_4 = (\text{area of CH}_4 \text{ peak from integrator plot on GC-14B}) \times 8 \times 10^{12} \quad (\text{iv})$$

APPENDIX F

PORE SIZE DISTRIBUTION CURVES

The pore size distribution curves derived from N₂ desorption from spherical silica and alumina-silica composites supports and their catalysts are illustrated in the following figures.

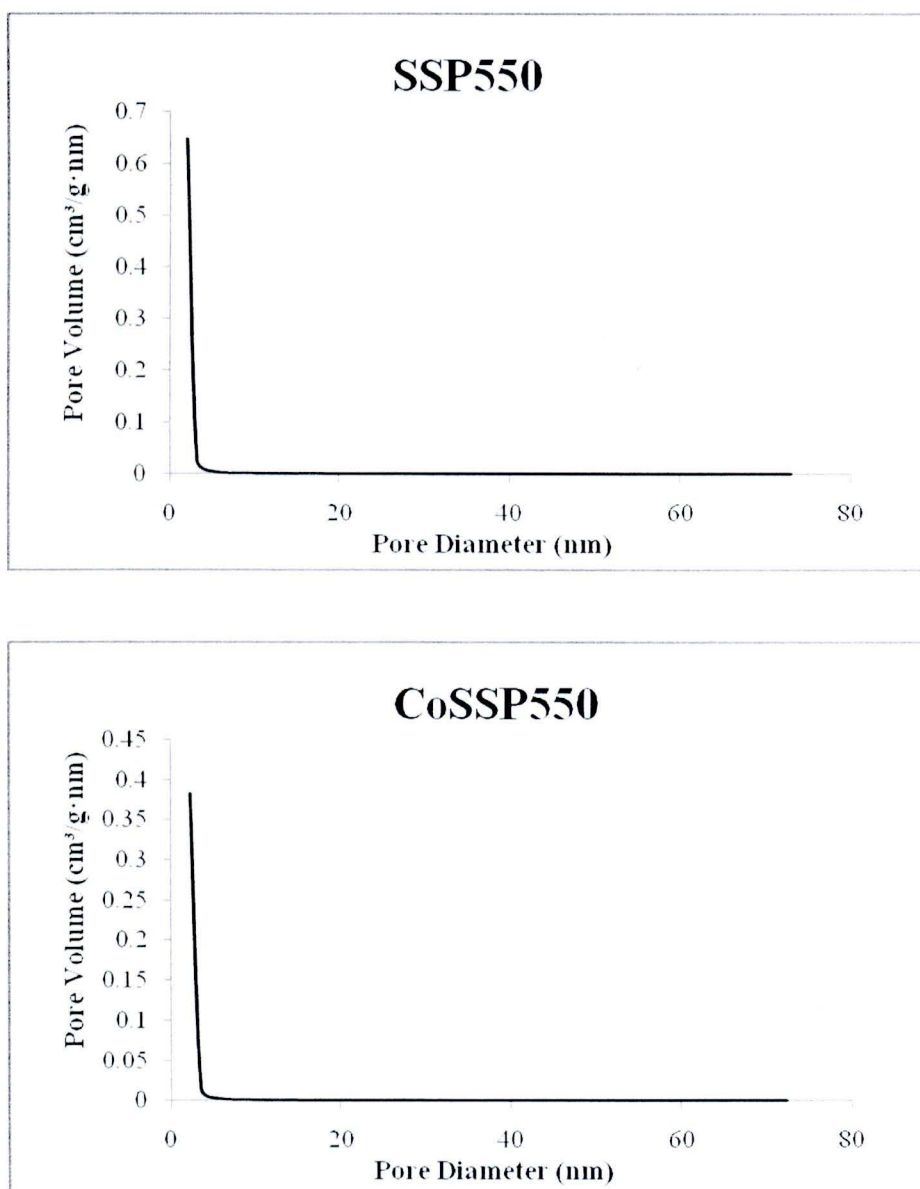


Figure F.1 The pore size distribution of SSP550 and CoSSP550.

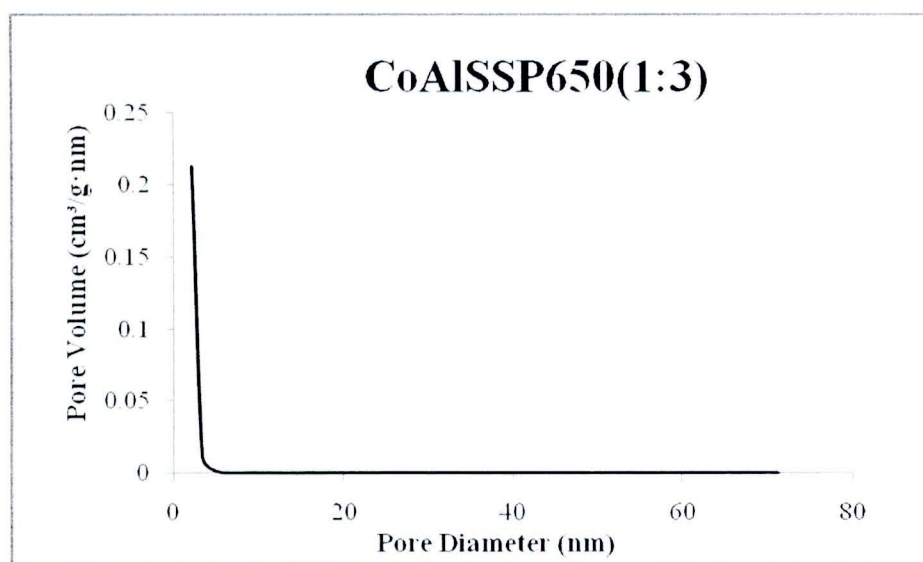
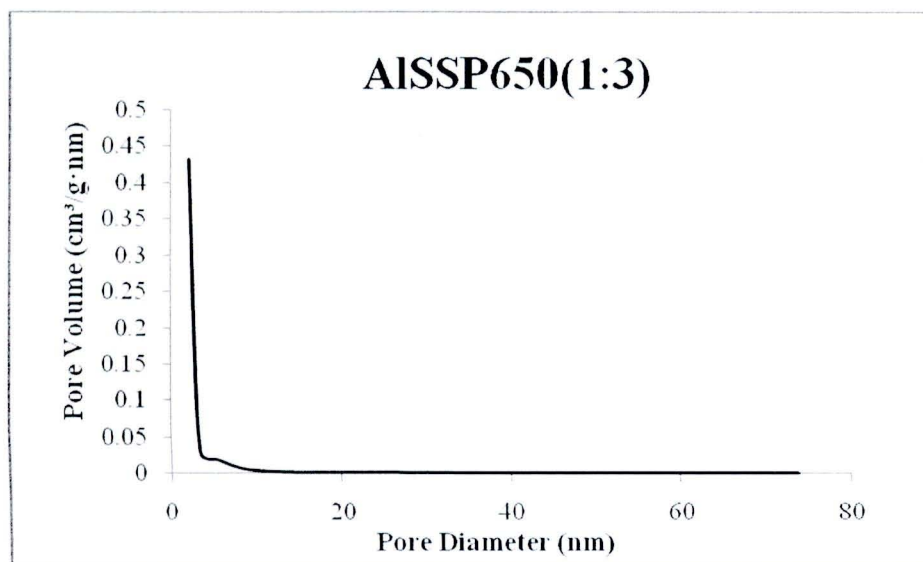


Figure F.2 The pore size distribution of AlSSP650 (1:3) and CoAlSSP650 (1:3).

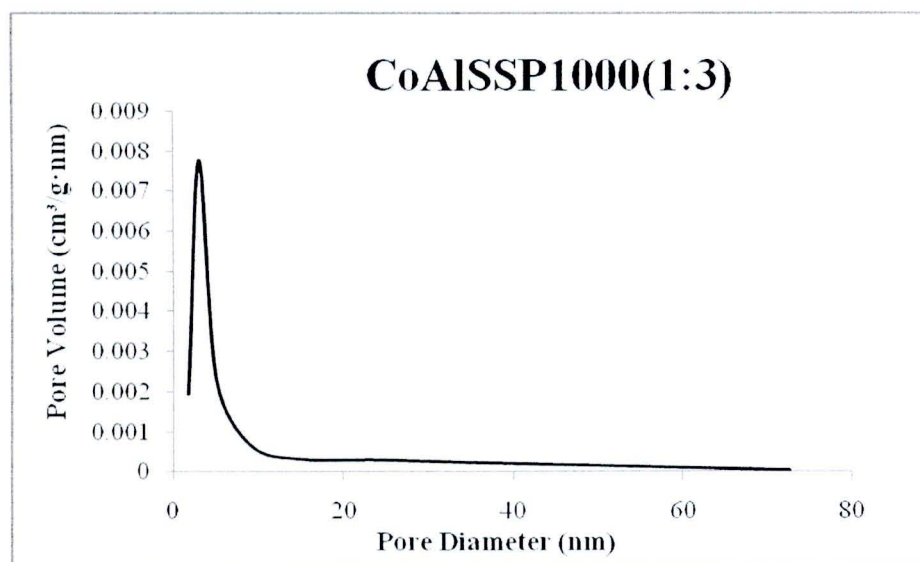
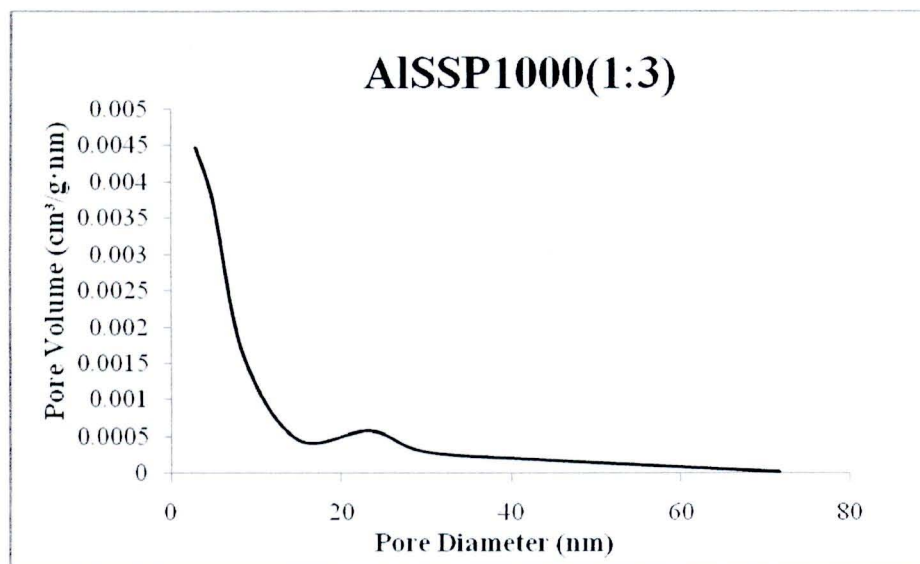


Figure F.3 The pore size distribution of AISSP1000 (1:3) and CoAISSP1000 (1:3).

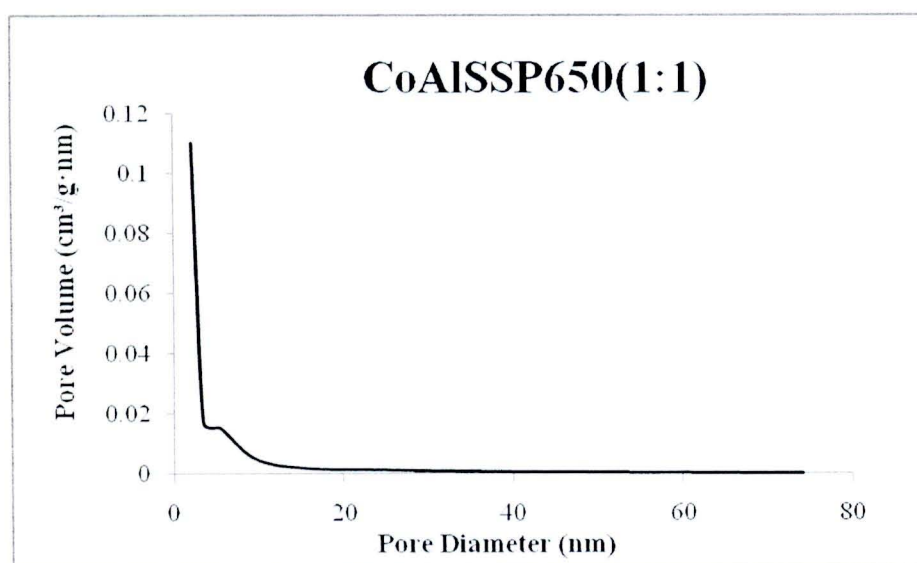
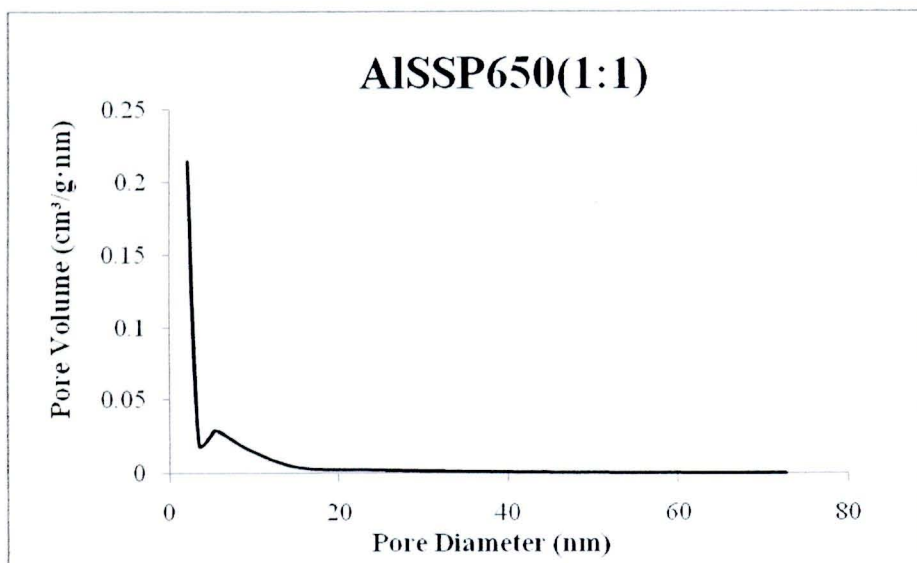


Figure F.4 The pore size distribution of AISSP650 (1:1) and CoAISSP650 (1:1).

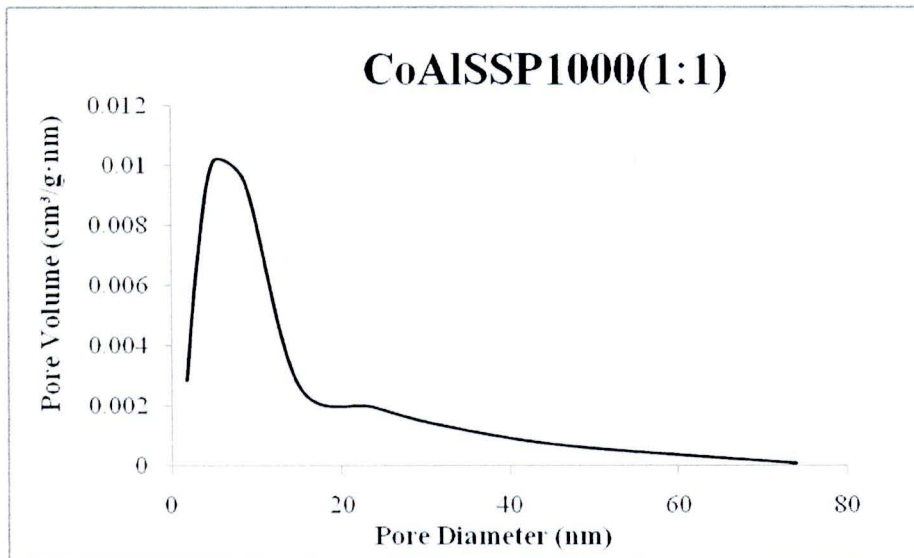
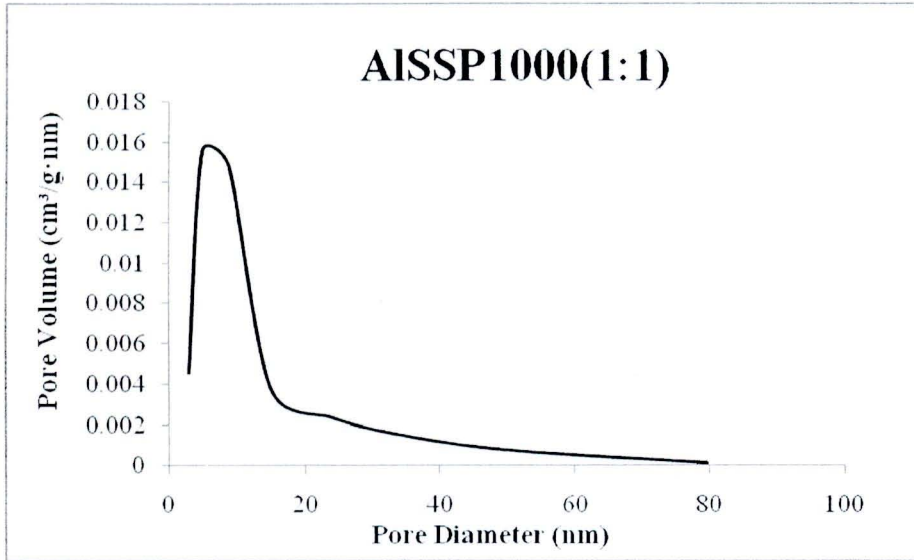


Figure F.5 The pore size distribution of AISSP1000 (1:1) and CoAISSP1000 (1:1).

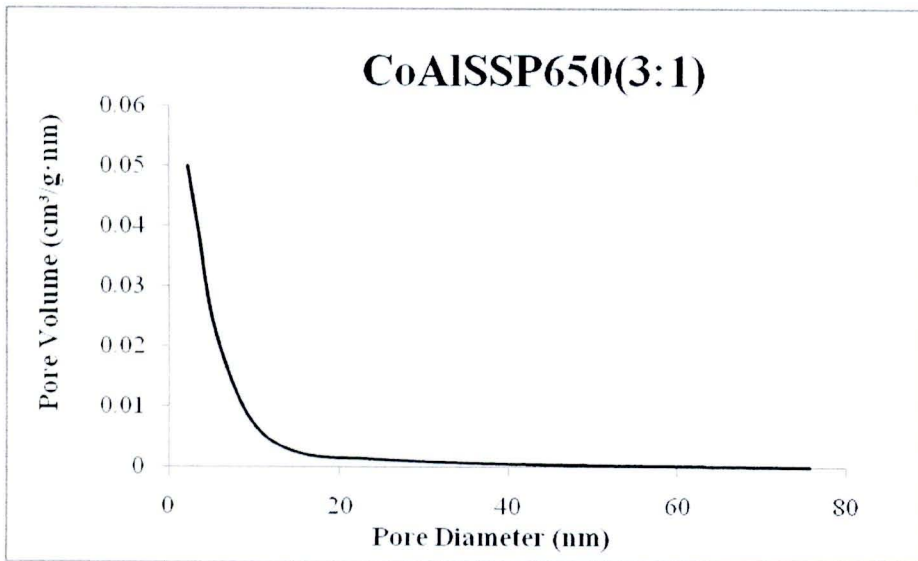
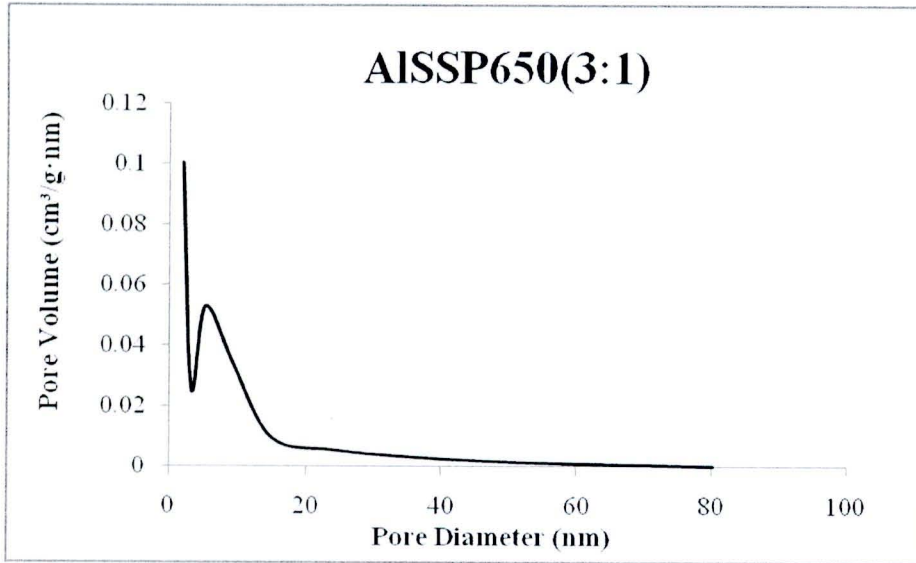


Figure F.6 The pore size distribution of AISSP650 (3:1) and CoAISSP650 (3:1).

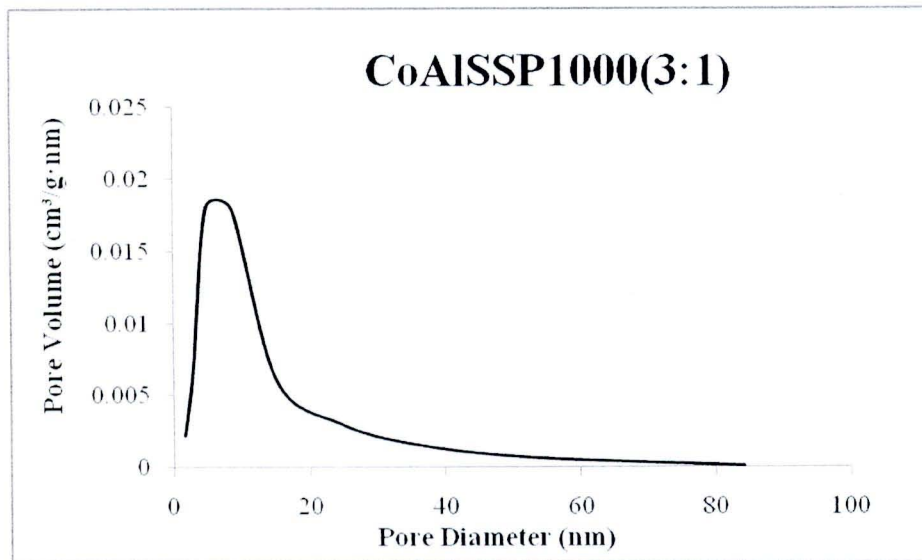
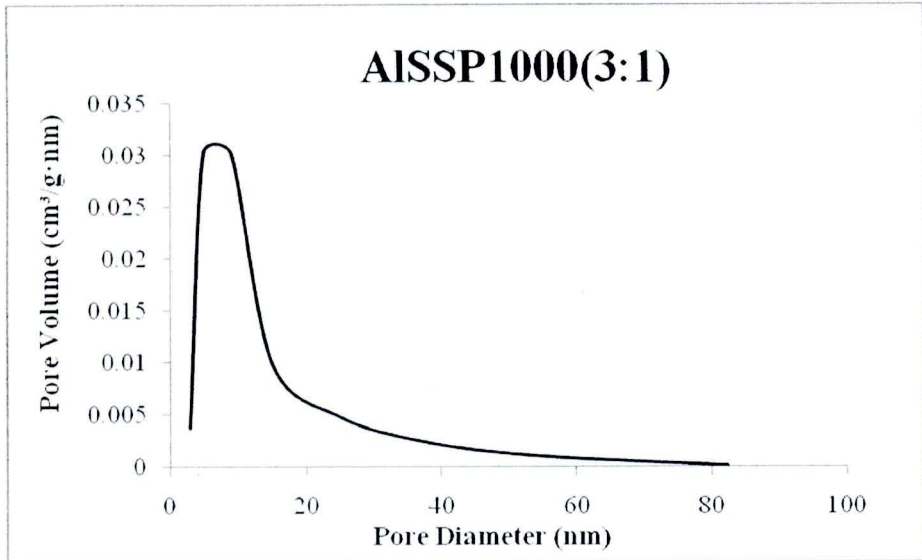


Figure F.7 The pore size distribution of AISSP1000 (3:1) and CoAISSP1000 (3:1).

VITA

Miss Thamonwan Jetsadanurak was born on November 21st, 1983 in Songkhla province, Thailand. She finished high school from Mahidolwittayanusorn School in 2002, and received the bachelor's degree of Chemical Technology from Chulalongkorn University in 2006. She continued her master's study at Department of Chemical Engineering, Faculty of Engineering, Chulalongkorn University in 2009.



