

REFERENCES

1. Bao, C., Ouyang, M., and Yi, B., 2006, "Modeling and Control of Air Stream and Hydrogen Flow with Recirculation in a PEM Fuel Cell System--I. Control-Oriented Modeling", **International Journal of Hydrogen Energy**, Vol. 31, No. 13, pp. 1879-1896.
2. Pathapati, P.R., Xue, X., and Tang, J., 2005, "A New Dynamic Model for Predicting Transient Phenomena in a PEM Fuel Cell System", **Renewable Energy**, Vol. 30, No. 1, pp. 1-22.
3. Xue, X., Tang, J., Smirnova, A., England, R., and Sammes, N., 2004, "System Level Lumped-Parameter Dynamic Modeling of PEM Fuel Cell", **Journal of Power Sources**, Vol. 133, No. 2, pp. 188-204.
4. Bao, J., Chan, K.H., Zhang, W.Z., and Lee, P.L., 2007, "An Experimental Pairing Method for Multi-Loop Control Based on Passivity", **Journal of Process Control**, Vol. 17, No. 10, pp. 787-798.
5. Barbir, F., 2005, " PEM Fuel Cells: Theory and Practice", **Elsevier Academic Press**, Vol.3, No. 6, pp. 45-56.
6. NA, W.K., 2008, **Dynamic Modeling, Control and Optimization of PEM Fuel Cell System for Automotive and Power System Applications** The University of Texas at Arlington, Texas, pp. 13-18.
7. Gou, W., 2007, "Nonlinear Control of PEM Fuel Cells by Exact Linearization", **IEEE Transaction on IAS (Industrial Application Systems)**, Vol. 43, No. 6, pp. 1426 - 1433.
8. Amphlett, J.C., Mann, R.F., Peppley, B.A., Roberge, P.R., and Rodrigues, A., "A Model Predicting Transient Responses of Proton Exchange Membrane Fuel Cells", **Journal of Power Sources**, Vol. 61, No. 1-2, pp. 183-188.
9. Wu, W., Xu, J.P., and Hwang, J.J., 2009, "Multi-Loop Nonlinear Predictive Control Scheme for a Simplistic Hybrid Energy System", **International Journal of Hydrogen Energy**, Vol. 34, No. 9, pp. 3953-3964.
10. Amphlett, J.C., Baumert, R.M., Mann, R.F., Peppley, B.A., Roberge, P.R., and Rodrigues, A., 1994, "Parametric Modelling of the Performance of a 5-Kw Proton-Exchange Membrane Fuel Cell Stack", **Journal of Power Sources**, Vol. 49, No. 1-3, pp. 349-356.
11. Sharifi Asl, S.M., Rowshanzamir, S., and Eikani, M.H., 2010, "Modelling and Simulation of the Steady-State and Dynamic Behaviour of a PEM Fuel Cell", **Energy**, Vol. 35, No. 4, pp. 1633-1646.
12. J. Purkrushpan, A.G.S., and H. Peng, 2002, Modeling and Control for PEM Fuel Cell Stack Systems. **Proc. Amer. Control Conf.**, Vol. 3, No. 2, pp. 33-46.
13. Labal, M., 2005, "Modeling and Analysis of Electro Chemical, Thermal, and Reactant Flow Dynamics for a PEM Fuel Cell System", **Fuel cells**, Vol. 4, No. 6, pp. 463-475.

14. M.P. Nielsen, P.P., C.A. Andesen, M.O. Christen, and A.R. Korgaard, 2002, **Design and Control of Fuel Cell System for Transport Application**, Aalborg University.
15. Chmielewski, K., 2006, "Power Control of a Polymer Electrolyte Membrane Fuel Cel", **Ind.Eng.Chem.Res.**, Vol. 45, No. 3, pp. 4661-4670.
16. Zhang, J., Tang, Y., Song, C., Xia, Z., Li, H., Wang, H., and Zhang, J., 2008, " PEM Fuel Cell Relative Humidity (Rh) and Its Effect on Performance at High Temperatures", **Electrochimica Acta**, Vol. 53, No. 16, pp. 5315-5321.
17. Friedland, B., 1987, **Control System Design 'an Introduction To State-Space Methods'**, McGraw-Hill Book Company, New York, pp. 322-325.
18. Bao, J., Zhang, W.Z., and Lee, P.L., 2003, "Decentralized Fault-Tolerant Control System Design for Unstable Processes", **Chemical Engineering Science**, Vol. 58, No. 22, pp. 5045-5054.
19. L.Y. Chiu, B., 2004, "An Improve Small-Signal Model of the Dynamic Behavior of PEM Fuel Cells ", **IEEE Trans. Industry Applications**, Vol. 40, No. 4, pp. 970–077.
20. Ahn, J.W. and Choe, S.Y., 2008, "Coolant Controls of a PEM Fuel Cell System", **Journal of Power Sources**, Vol. 179, No. 1, pp. 252-264.
21. WenZ, Z. and Peter, L., 2002, "Decentralized Unconditional Stability Conditions Based on the Passivity Theorem for Multi-Loop Control Systems", **Ind.Eng.Chem.Res.**, Vol. 41, pp. 1569-1578.
22. Bao, J., 2002, "Passivity-Based Decentralized Failure-Tolerant Control", **Ind. Eng. Chem. Res.**, Vol. 41, No. 23, pp. 5702-5715.
23. Lebbal, M.E. and Lecoeuche, S., 2009, "Identification and Monitoring of a PEM Electrolyser Based on Dynamical Modelling", **International Journal of Hydrogen Energy**, Vol. 34, No. 14, pp. 5992-5999.
24. Luis A.M., 2008, Controlling PEM Fuel Cells Applying a Constant Humidity Technique **ABCM Symposium Series in Mechatronics**, Vol. 3, pp. 774-783.



APPENDIX A

Numeric value

A.1 Constant value

Anode volume(V_{an})	=	0.005 m^3
Anode flow constant (k_{an})	=	0.065 mol/s atm
Cathode Volume (V_{cat})	=	0.01 m^3
Cathode flow constant (k_{cat})	=	0.065 mol/s atm
Faraday's constant (F)	=	96485 A.s/mol
Gas constant (R)	=	$8.206 \times 10^{-5} \text{ m}^3 \text{ atm/mol K}$
Hydrogen pressure inlet ($P_{H_2,in}$)	=	3 atm
Number of fuel cell stack (N)	=	35
Oxygen pressure outlet ($P_{O_2,out}$)	=	1 atm

A.2 Normal operating value

Current load (I)	=	100 A
Hydrogen flowrate ($\dot{m}_{H_2,in}$)	=	0.008 mol/s
Oxygen flowrate ($\dot{m}_{O_2,in}$)	=	0.02 mol/s

A.3 Steady state value

Cell voltage (\bar{V}_{cell})	=	27.5 V
Hydrogen pressure (\bar{P}_{H_2})	=	2.74 atm
Oxygen pressure (\bar{P}_{O_2})	=	3.16 atm
Stack temperature (\bar{T}_s)	=	75 C

APPENDIX B

Source code

B.1 The steady state value

This section is used to find the steady state values used in the proton exchange membrane fuel cell.

```
clc
clear
format long
```

```
%%The partial pressure of hydrogen
syms pH2
H2inlet=0.008; %mol/s
kan=0.065; %mol/s.atm
pH2in=2.9; %atm
N=35;
I=100; %A
F=96485; %A.s/mol
ANS=solve(H2inlet-kan*(pH2-pH2in)-(N*I/2/F));
pH2_ss=double(ANS)
```

```
%%The partial pressure of oxygen
syms pO2
O2inlet=0.02; %mol/s
kcat=0.065; %mol/s.atm
patm=3 ; %atm
N=35;
I=100; %A
F=96485; %A.s/mol
ANS=solve(O2inlet-kcat*(pO2-patm)-(N*I/4/F));
pO2_ss=double(ANS)
```

```
%%The stack temperature
syms T
CpH2=14209; %J/kg.K
CpO2=922; %J/kg.K
Cpw=4184; %J/kg.K
Ct=17.9*1000; %J/K
T0=298.15; %K
Tamb=298.15; %K
Tc=298.15; %K
MwH2=2.016; %kg/kmol
MwO2=32; %kg/kmol
MwH2O=18; %kg/kmol
kconv_an=2; %J/s.K
kconv_cat=10; %J/s.K
```

```

kconv_amb=17;           %J/s.K
Vcell=0.7552;          %V
Hreact=285.5*1000;     %J/mol
Mcw=0.45;               %mol/s
Van=0.005;              %m^3
Vcat=0.01;               %m^3
R=8.205746e-5;         %m^3 atm/mol K
Tstack=(kconv_amb*(Tamb-T))+(N*I/2/F*Hreact)-(35*Vcell*I)-
(Mcw*Cpw*MwH2O*(T-Tc)/1000);
ANS=solve(Tstack);
T_ss=double(ANS)
T_ss_celcius=T_ss-273.15

%%The cell voltage and power
e1=-0.944;
e2=3.54E-3;
e3=-1.96e-4;
e4=7.8e-5;
e5=3.3e-3;
e6=-7.55e-6;
e7=1.1e-6;
I=100;                  %A
Enert=1.229-((8.5E-4)*(T_ss-298.15))+((4.308E-
5)*T_ss*(log(pH2_ss)+log(0.5*pO2_ss)));
cO2=pO2_ss/((5.08e6)*exp(-498/T_ss));
act=e1+(e2*T_ss)+(e3*T_ss*log(I))+(e4*T_ss*log(cO2));
ohm=-I*(e5+(e6*T_ss)+(e7*I));
Vcell=Enert+act+ohm
Power=Vcell*I           %watt

```

B.2 Finding A,B,C,D, E and system transfer function matrix

```

%%Finding A matrix
A11=-kan*R*T_ss/Van;
A13=R/Van*(H2inlet-kan*(pH2_ss-pH2in)-(N*I/2/F));
A22=-kcat*R*T_ss/Vcat;
A23=R/Vcat*(O2inlet-kcat*(pO2_ss-patm)-(N*I/4/F));
A33=-(kconv_amb+(Mcw*Cpw*MwH2O/1000))/Ct;
A=[A11 0 A13;0 A22 A23;0 0 A33]

```

```

%%Finding B matrix
B11=R*T_ss/Van;
B22=R*T_ss/Vcat;
B33=-Cpw*MwH2O/1000*(T_ss-Tc)/Ct;

```

```

B=[B11 0 0;0 B22 0;0 0 B33]

%%Finding C matrix
C=[1 0 0;0 1 0;0 0 1]

%%Finding D matrix
D_process=[0 0 0;0 0 0;0 0 0]
D_dis=[0;0;0]

%%Finding E matrix
E11=-R*T_ss*N/Van/2/F;
E21=-R*T_ss*N/Vcat/4/F;
E31=((N*Hreact/2/F)-(35*Vcell))/Ct;
E=[E11;E21;E31]

%%Finding transfer function matrix
system=ss(A,B,C,D)
g=tf(system)

```

B.3 Finding passivity index

```

%%Finding passivity index
w = logspace(-4,4,200)
s = w * sqrt(-1) %s = jw
I = eye(length (A)) %I = identity matrix
for z=1:length(s)
g= C*((s(z)*I-A)\B)+D; %g = transfer function
greal = real(Gplus);
gimag = imag(Gplus);

%size of new matrix
[nAr,nAc] = size(greal);
[nBr,nBc] = size(gimag);

% -----LMI-#1-----
setlmis([]);
DE = lmivar(1,[ones(nAr,2)]);
lmiterm([1 1 1 0],eye(nAr)); %LMI #1: eye(nAr)
lmiterm([-1 1 1 DE],1,1); %LMI #1: DE
lmiterm([1 1 1 DE],greal,-1,'s'); %LMI #2: -greal*DE-DE*greal'
lmiterm([1 2 1 DE],1,gimag'); %LMI #2: DE*gimag'
lmiterm([1 2 1 DE],gimag,-1); %LMI #2: -gimag*DE
lmiterm([1 2 2 DE],greal,-1,'s'); %LMI #2: -greal*DE-DE*greal'
lmiterm([-1 1 1 DE],1,1); %LMI #2: DE

```

```

lmiterm([-1 2 1 0],zeros(nAr));      %LMI #2: zeros(nAr)
lmiterm([-1 2 2 DE],1,1);          %LMI #2 DE
sys = getlmis;

% ----- Generalized Eigenvalue Minimization of t #2-----
[tmin,Xopt] = gevp(sys,1);
Dm = dec2mat(sys,Xopt,DE);
DNew = sqrt(Dm);
DGp = inv(DNew)*Gplus*DNew;
nu= -min(real(eig(DGp+DGp')))/2;
end
disp('t is '); disp(tmin);
disp('Dm is '); disp(Dm);

% %Plot passivity index
figure(1);
semilogx(w,nu,'bl-.');
xlabel('Frequency (rad/hr)');
ylabel('Passivity Index');
legend('Passivity index of PEMFC system');
grid;

```

B.4 Finding the weighting function

```

%%Finding weighting function of PEMFC system
%To find the parameters of weighting function (a,b,c and k), this file must be opened
open with
myfun.m and mynoncon.m file
options = optimset('Display','iter','MaxFunEvals',100000);
[x,fval] = fmincon(@myfun,[9.234 3.2687 0.081 0.5558],[],[],[],[],[0 0 0 0],[100 100
100 1],@mynoncon,options,nu,w)
ww01 = x(1)
ww02 = x(2)
ww03 = x(3)
ww04 = x(4)
%%The transfer function and passivity index of weighting function
WtfnG=tf([x(4) x(1)*x(4) 0], {[1 x(2)+x(3) x(2)*x(3)]});
for z=1:length(w)
Gwt = freqresp(WtfnG,w(z));
nu1(z)= -min(real(eig(Gwt+Gwt')))/2;
end

%%Plot passivity index of weighting function
figure(2);

```

```

semilogx(w,nul,'r-');
xlabel('Frequency (rad/hr)');
ylabel('Passivity index');
legend('passivity Index of weighting functionp');
% grid;

```

B.5 Making the PEMFC is passive process

After the weighting function is obtained, it is added into the non-passive system to make it passive system

```

%%Add the weighting into the PEMFC system
for z = 1:length(w)
Gp1 = C*(((s(z)*I)-A)\B) + D ;
Gplus = Gp1;
wf = (x(4).*(w(z).*i).*((w(z).*i)+x(1)))/(((w(z).*i)+x(2)).*((w(z).*i)+x(3)));
Wtfn = wf*I; %weighting function matrix
H =Gplus+Wtfn %Transfer function after adding the weighting
function
nu2(z)= -min(real(eig(H+H'))/2); %passivity index of passive system
end

```

```

%%Finding passivity index of passive system
for z = 1:length(w)
Gp1 = C*(((s(z)*I)-A)\B) + D ;
Gplus = Gp1;
wf = (x(4).*(w(z).*i).*((w(z).*i)+x(1)))/(((w(z).*i)+x(2)).*((w(z).*i)+x(3)));
Wtfn = wf*I; %weighting function matrix
H =Gplus+Wtfn %Transfer function after adding the weighting
function
nu2(z)= -min(real(eig(H+H'))/2); %passivity index of passive system
ggreal = real(H);
ggimag = imag(H);

```

```

%size of new matrix
[nAAr,nAAc] = size(ggreal);
[nBBr,nBBC] = size(ggimag);
setlmis([]);
DE = lmivar(1,[ones(nAAr,2)]);
lmiterm([1 1 1 0],eye(nAAr)); %LMI #1: eye(nAAr)
lmiterm([-1 1 1 DE],1,1); %LMI #1: DE
lmiterm([1 1 1 DE],ggreal,-1,'s'); %LMI #2: -ggreal*DE-DE*ggreal'
lmiterm([1 2 1 DE],1,ggimag'); %LMI #2: DE*ggimag'
lmiterm([1 2 1 DE],ggimag,-1); %LMI #2: -ggimag*DE

```

```

lmiterm([1 2 2 DE],ggreal,-1,'s');    %LMI #2: -ggreal*DE-DE*ggreal'
lmiterm([-1 1 1 DE],1,1);             %LMI #2: DE
lmiterm([-1 2 1 0],zeros(nAAr));     %LMI #2: zeros(nAAr)
lmiterm([-1 2 2 DE],1,1);             %LMI #2 DE
sys2 = getlmis;

%----- Generalized Eigenvalue Minimization of t #2
[tmin2,Xopt2] = gevp(sys2,1);
Dm2 = dec2mat(sys2,Xopt2,DE);
DNew2 = sqrt(Dm2);
DGp2 = inv(DNew2)*H*DNew2;
nu3(z) = -min(real(eig(DGp2+DGp2'))/2);
end

%%Plot passivity index of passive system
figure(3);
semilogx(w,nu3,'r-');
xlabel('Frequency (rad/hr)');
ylabel('Passivity index of passive system');
legend('');
grid;

```

B.6 Finding the PI-controller

%To find the parameters of PI-controller ($k_{c,i}^+$ and $\tau_{I,i}$), this file must be opened open with

myfunpi.m and mynonconpi.m file

```

%% The parameters for loop1  $m_{H_2,m} - P_{H_2}$ 
for z=1:length(w)
gPI = C*(((w(z).*i).*I)-A)\B) + D;
wf = (x(4).*w(z).*i).*((w(z).*i)+x(1)))/(((w(z).*i)+x(2)).*((w(z).*i)+x(3)));
Wtfn = wf*I;
U = [1 0 0;0 1 0;0 0 1];
gPIplus = gPI.*U;
H =gPIplus+Wtfn ;
GLoop1=H(1,1);
options = optimset('Display','iter','MaxFunEvals',10000);
[p,fval] =fmincon(@myfunpi,[0.00005 0.001 20],[],[],[],[],[0.0000000001 0.001
19],[1500 0.001 20],@mynonconpi,options,nu3,GLoop1,w,z);
gamma1=[p(1)]
kcplus1=[p(2)]
ti1=[p(3)]

```



end

```
%% The parameters for loop2  $\dot{m}_{O_{2,in}} - P_{O_2}$ 
for z=1:length(w)
gPI = C*(((w(z).*i).*I)-A)\B) + D;
wf = (x(4).*w(z).*i).*((w(z).*i)+x(1)))/((w(z).*i)+x(2)).*((w(z).*i)+x(3)));
% Wtfn = wf*I;
U = [1 0 0;0 1 0;0 0 1];
gPIplus = gPI.*U;
H =gPIplus+Wtfn ; %Transfer function after adding the weighting function
GLoop1=H(2,2);
options = optimset('Display','iter','MaxFunEvals',10000);
[p,fval] =fmincon(@myfunpi,[0.00005 0.001 20],[],[],[],[],[0.0000000001 0.001
19],[1500 0.001 20],@mynonconpi,options,nu3,GLoop1,w,z);
gamma2=[p(1)]
kcplus2=[p(2)]
ti2=[p(3)]
end
```

%% The parameters for loop3 $\dot{m}_{cv} - T_s$

```
for z=1:length(w)
gPI = C*(((w(z).*i).*I)-A)\B) + D;
wf = (x(4).*w(z).*i).*((w(z).*i)+x(1)))/((w(z).*i)+x(2)).*((w(z).*i)+x(3)));
Wtfn = wf*I;
U = [1 0 0;0 1 0;0 0 1];
gPIplus = gPI.*U;
H =gPIplus+Wtfn ;
GLoop1=H(3,3);
options = optimset('Display','iter','MaxFunEvals',10000);
[p,fval] =fmincon(@myfunpi,[0.00005 0.011487 0.000907],[],[],[],[],[0.0000000001
0.011387 0.000907],[1500 0.011487
0.000917],@mynonconpi,options,nu3,GLoop1,w,z);
gamma3=[p(1)]
kcplus3=[p(2)]
ti3=[p(3)]
end
```

B.7 The added files for finding the weighting function

```
%%Myfun
function f = myfun(x,nu,w)
for z=1:length(w)
s = w(z)*i;
```

```

wp(z) = (x(4)*s*(s+x(1)))/((s+x(2))*(s+x(3)));
fnction(z) = (real(wp(z))-nu2(z))^2;
end
f = sum(fnction);
end

```

```

%%MyNoncon
function [c, ceq] = mynoncon(x,nu,w)
for z=1:length(w)
s = w(z)*i;
wp(z) = (x(4)*s*(s+x(1)))/((s+x(2))*(s+x(3)));
end
c = nu2-real(wp);      %inequality constraint
ceq=[];
end

```

B.8 The added files for finding the PI-controller

```

%%MyFunPI
function f = myfunpi(p,nu,GLoop1,w,z)
f= -1*p(1);
end

%%MyNonConPI
function [c, ceq] = mynonconpi(p,nu,GLoop1,w,z)
a = 1+GLoop1.*p(2).*(1+(1./(p(3).*w.*i)));
c(1)=max(abs(p(1)./(a.*w.*i))-1;
c(2)=-min(real((p(2).*(1+(1./(p(3).*w.*i))))./((1-((p(2).*(1+(1./(p(3).*w.*i)))).*nu)))));
ceq=[];
end

```

CURRICULUM VITAE

NAME Miss Nichaporn Kanjanabat

DATE OF BIRTH 14 September 1986

EDUCATIONAL RECORD

HIGH SCHOOL	High School Graduation Assumption Suksa School, 2005
BACHELOR'S DEGREE	Bachelor of Engineering (Chemical Engineering) King Mongkut's University of Technology Thonburi, 2008
MASTER'S DEGREE	Master of Engineering (Chemical Engineering) King Mongkut's University of Technology Thonburi, 2010

**King Mongkut's University of Technology Thonburi
Agreement on Intellectual Property Rights Transfer for Postgraduate Students**

Date 27 April 2011

Name Nichaporn Middle Name -

Surname/Family Name Kanjanabat

Student Number 52403805 who is a student of King's Mongkut's University of Technology Thonburi (KMUTT) in Graduate Diploma Master Degree
 Doctoral Degree

Program Chemical Engineering Practice School Field of Study Chemical Engineering
Faculty/School Engineering

Home Address 152 Soi Putabucha 36 Road Putabucha
Tambon Bangmod District Thrungru Province Bangkok
Postal Code 10140 Country Thailand

I, as 'Transferer', hereby transfer the ownership of my special research project copyright to King's Mongkut's University of Technology Thonburi who has appointed Assoc. Prof. Dr. Piyabutr Wanichpongpan Associate Dean for Academic Affairs (Acting for Dean) to be 'Transferee' of copyright ownership under the 'Agreement' as follows.

1. I am the author of the special research project entitled Stability analysis of proton exchange membrane fuel cell under the supervision of Assoc. Prof. Dr. Thongchai Srinophakun who is my supervisor, in accordance with the Thai Copyright Act B.E. 2537. The special research project is a part of the curriculum of KMUTT.

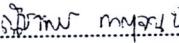
2. I hereby transfer the copyright ownership of all my works in the special research project to KMUTT throughout the copyright protection period in accordance with the Thai Copyright Act B.E. 2537, effective on the approval date of special research project proposal consented by KMUTT.

3. To have the special research project distributed in any form of media, I shall in each and every case stipulate the special research project as the work of KMUTT.

4. For my own distribution of special research project or the reproduction, adjustment, or distribution of special research project by the third party in accordance with the Thai Copyright Act B.E. 2537 with remuneration in return, I am subject to obtain a prior written permission from KMUTT.

5. To use any information from my special research project to make an invention or create any intellectual property works within ten (10) years from the date of signing this Agreement, I am subject to obtain prior written permission from KMUTT, and KMUTT is entitled to have intellectual property rights on such inventions or intellectual property works, including entitling to take royalty from licensing together with the distribution of any benefit deriving partly or wholly from the works in the future, conforming with the Regulation of King Mongkut's Institute of Technology Thonburi Re the Administration of Benefits deriving from Intellectual Property B.E. 2538.

6. If the benefits arise from my special research project or my intellectual property works owned by KMUTT, I shall be entitled to gain the benefits according to the allocation rate stated in the Regulation of King Mongkut's Institute of Technology Thonburi Re the Administration of Benefits Arising from Intellectual Property B.E. 2538.

Signature..... Transferor

(Miss Nichaporn Kanjanabat)

Student

Signature..... Transferee

(Assoc. Prof. Dr. Piyabutr Wanichpongpan)

Associate Dean for Academic Affairs (Acting for Dean)

Signature..... Witness

(Assoc. Prof. Dr. Anawat Sungpet)

Signature..... Witness

(Assoc. Prof. Dr. Thongchai Srinophakun)



